Staggered discretizations, pressure corrections schemes and all speed flows

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Introduction

Continuous problem

Euler (Navier-Stokes) equations:

$$\begin{aligned} \partial_t \varrho + \operatorname{div}(\varrho \boldsymbol{u}) &= 0, \\ \partial_t(\varrho \boldsymbol{u}) + \operatorname{div}(\varrho \boldsymbol{u} \otimes \boldsymbol{u}) - \operatorname{div} \boldsymbol{\tau} + \boldsymbol{\nabla} \boldsymbol{p} &= 0 \\ \partial_t(\varrho \boldsymbol{E}) + \operatorname{div}\left[(\varrho \boldsymbol{E} + \boldsymbol{p})\boldsymbol{u}\right] &= \operatorname{div}(\boldsymbol{\tau}\boldsymbol{u}), \\ \boldsymbol{p} &= (\gamma - 1) \ \varrho \boldsymbol{e}, \quad \boldsymbol{E} &= \frac{1}{2} |\boldsymbol{u}|^2 + \boldsymbol{e}. \end{aligned}$$

For regular functions, taking the inner product of the momentum balance equation by u and using the mass balance equation yields the kinetic energy balance equation:

$$\partial_t(\varrho E_c) + \operatorname{div}(\varrho E_c \boldsymbol{u}) + \boldsymbol{\nabla} \boldsymbol{p} \cdot \boldsymbol{u} = \operatorname{div}(\boldsymbol{\tau}) \cdot \boldsymbol{u}, \qquad E_c = \frac{1}{2} |\boldsymbol{u}|^2.$$

Subtracting to the total energy balance yields the internal energy balance:

$$\partial_t(\varrho e) + \operatorname{div}(\varrho e u) + p \operatorname{div} u = \tau : \nabla u,$$

and, from this equation, we get $e \ge 0$.

• Estimates satisfied by the solution: $\varrho \ge 0$, $e \ge 0$, $\int_{\Omega} \varrho = \int_{\Omega} \varrho_0$, $\int_{\Omega} \varrho E = \int_{\Omega} \varrho_0 E_0$.

Introduction

Objectives (1/2)

Derive a scheme for Euler (or Navier-Stokes) equations:

- (i) unconditionnally stable (i.e. same estimates as in the continuous case),
- (ii) accurate at all Mach numbers,
- (iii) which converges to the correct weak (discontinuous) solutions.
 - (ii) suggests to use a staggered discretization (iv), and to perform upwinding (if any) with respect to the material velocity.
 - ▶ (i) and (iv) suggest to solve the internal energy balance:
 - keep e positive, • e and $\frac{1}{2}|u|^2$ are not discretized at the same place.
 - (i) will be a constraint for the choice of the time-stepping algorithm: implicit scheme or pressure correction method.

So a staggered scheme, solving the internal energy balance, upwind/u.

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ISIS: https://gforge.irsn.fr/gf/project/isis
PELICANS: https://gforge.irsn.fr/gf/project/pelicans
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o n e



- Morality: "Consider a conservative scheme. Suppose that a sequence of discrete solutions converges. Then the limit is a weak solution."
- So how to obtain the correct weak solutions of Euler equations while solving the internal energy balance ?

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A colocated scheme (1/7)



- Mass balance $(\partial_t(\varrho) + \operatorname{div}(\varrho u) = 0)$:
 - Velocity at the face $\sigma = K | L$:

$$\boldsymbol{u}_{\sigma} = \frac{d_{L,\sigma}}{d_{\sigma}}\boldsymbol{u}_{K} + \frac{d_{K,\sigma}}{d_{\sigma}}\boldsymbol{u}_{L}, \qquad d_{K,\sigma} = d(\boldsymbol{x}_{K},\sigma), \ d_{L,\sigma} = d(\boldsymbol{x}_{L},\sigma), \ d_{\sigma} = d(\boldsymbol{x}_{K},\boldsymbol{x}_{L}).$$

▶ Mass flux : $F_{K,\sigma} = |\sigma| \rho_{\sigma} u_{\sigma} \cdot \boldsymbol{n}_{K,\sigma}$, with ρ_{σ} the upwind value of the density at the face.

• Mass balance:
$$\frac{|K|}{\delta t} (\varrho_K - \varrho_K^*) + \sum_{\sigma = K|L} F_{K,\sigma} = 0$$

(IRSN/LATP)

Pressure corr. schemes and all speed flows

A colocated scheme

A colocated scheme (2/7)

• Building convection operators $z \mapsto \partial_t(\varrho z) + \operatorname{div}(\varrho z u)$ from the mass balance:

$$\frac{|K|}{\delta t} \left(\varrho_{K} - \varrho_{K}^{*} \right) + \sum_{\sigma = |K|} F_{K,\sigma} = 0.$$

Then (1) the centered operator:

$$(C\boldsymbol{u})_{K} = \frac{1}{\delta t} \left(\varrho_{K} \boldsymbol{u}_{K} - \varrho_{K}^{*} \boldsymbol{u}_{K}^{*} \right) + \frac{1}{|K|} \sum_{\sigma = K|L} F_{K,\sigma} \boldsymbol{u}_{\sigma}, \qquad \boldsymbol{u}_{K|L} = \frac{1}{2} \left(\boldsymbol{u}_{K} + \boldsymbol{u}_{L} \right)$$

satisfies:

$$(C\boldsymbol{u})_{K} \cdot \boldsymbol{u}_{K} = \frac{|K|}{2\delta t} \left(\varrho_{K} |\boldsymbol{u}_{K}|^{2} - \varrho_{K}^{*} |\boldsymbol{u}_{K}^{*}|^{2} \right) + \frac{1}{2} \sum_{\sigma = K|L} F_{K,\sigma} \boldsymbol{u}_{K} \boldsymbol{u}_{L} + \frac{|K|}{2\delta t} \varrho_{K}^{*} |\boldsymbol{u}_{K} - \boldsymbol{u}_{K}^{*}|^{2}.$$

Then (2) the upwind operator:

$$(Ce)_{\mathcal{K}} = \frac{1}{\delta t} \left(\varrho_{\mathcal{K}} e_{\mathcal{K}} - \varrho_{\mathcal{K}}^* e_{\mathcal{K}}^* \right) + \frac{1}{|\mathcal{K}|} \sum_{\sigma = \mathcal{K} | L} F_{\mathcal{K}, \sigma} e_{\sigma},$$

with an upwind choice for e_{σ} satisfies a discrete maximum principle.

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Pressure corr. schemes and all speed flows

A colocated scheme (3/7)

• Momentum balance $(\partial_t(\rho u) + \operatorname{div}(\rho u \otimes u) + \nabla p = 0)$:

$$|K|\Big[(C\boldsymbol{u})_{K}+(\boldsymbol{\nabla}p)_{K}-(\varepsilon\Delta\boldsymbol{u})_{K}\Big]=0.$$

- Centered convection term
- Pressure gradient designed to be the dual operator of the divergence:

$$(\boldsymbol{\nabla} \boldsymbol{p})_{\boldsymbol{K}} = \frac{1}{|\boldsymbol{K}|} \sum_{\sigma = \boldsymbol{K}|\boldsymbol{L}} |\sigma| \ \boldsymbol{p}_{\sigma} \ \boldsymbol{n}_{\boldsymbol{K},\sigma}, \qquad \boldsymbol{p}_{\boldsymbol{K}|\boldsymbol{L}} = \frac{d_{\boldsymbol{K},\sigma}}{d_{\sigma}} \boldsymbol{p}_{\boldsymbol{K}} + \frac{d_{\boldsymbol{L},\sigma}}{d_{\sigma}} \boldsymbol{p}_{\boldsymbol{L}}.$$

A diffusion term is added for stabilisation:

$$-(\varepsilon \Delta \boldsymbol{u})_{K} = \frac{1}{|K|} \sum_{\sigma=K|L} \varepsilon_{\sigma} \frac{|\sigma|}{d_{\sigma}} (\boldsymbol{u}_{K} - \boldsymbol{u}_{L}).$$

Upwind discretization of the convection term: $\varepsilon_{\sigma} = \frac{d_{\sigma}}{2} | \boldsymbol{u}_{\sigma} \cdot \boldsymbol{n}_{K,\sigma} |.$

A colocated scheme (4/7)

▶ Internal energy balance $(\partial_t(\varrho e) + \operatorname{div}(\varrho e u) + p \operatorname{div} u = 0)$:

$$|\mathcal{K}| (Ce)_{\mathcal{K}} + (\gamma - 1)\varrho_{\mathcal{K}} e_{\mathcal{K}}^{+} \sum_{\sigma = \mathcal{K}|L} |\sigma| \boldsymbol{u}_{\sigma} \cdot \boldsymbol{n}_{\mathcal{K},\sigma} = \boldsymbol{S}_{\mathcal{K}},$$

with $e_{K}^{+} = \max(e_{K}, 0)$ and S_{K} is a numerical source term.

- Upwind convection term.
- If the solutions exists, and if $S_K \ge 0$, e > 0.
- ▶ \exists at least a solution (topological degree argument), and, for this solution, $e^+ = e$ (the scheme is consistent).

A colocated scheme (5/7)

 S_K ?

- Strategy: try to build a (conservative) discrete total energy balance equation.
- Kinetic energy balance, without diffusion ($\varepsilon = 0$):

 $(\partial_t(\varrho E_c) + \operatorname{div}(\varrho E_c \boldsymbol{u}) + \boldsymbol{u} \cdot \boldsymbol{\nabla} p = 0, \ E_c = \frac{1}{2}|\boldsymbol{u}|^2)$

▶ Multiply the momentum balance equation by u_K and use the mass balance:

$$\frac{|\mathcal{K}|}{2\delta t} \left(\varrho_{\mathcal{K}} |\boldsymbol{u}_{\mathcal{K}}|^2 - \varrho_{\mathcal{K}}^* |\boldsymbol{u}_{\mathcal{K}}^*|^2 \right) + \frac{1}{2} \sum_{\sigma = \mathcal{K}|L} F_{\mathcal{K},\sigma} \boldsymbol{u}_{\mathcal{K}} \boldsymbol{u}_L + (\boldsymbol{\nabla}\rho)_{\mathcal{K}} \cdot \boldsymbol{u}_{\mathcal{K}} = \boldsymbol{R}_{\mathcal{K}}.$$

▶ Then, adding to the internal energy balance yields a total energy balance $(\partial_t(\rho E) + \operatorname{div}(\rho E u) + \operatorname{div}(\rho u) = 0)$:

$$\frac{|K|}{\delta t} \left(\varrho_{K} \boldsymbol{E}_{K} - \varrho_{K}^{*} \boldsymbol{E}_{K}^{*} \right) + \sum_{\sigma = K|L} \boldsymbol{F}_{K,\sigma} \boldsymbol{E}_{\sigma} + \sum_{\sigma = K|L} |\sigma| \ (\boldsymbol{p}\boldsymbol{u})_{\sigma} \cdot \boldsymbol{n}_{K,\sigma} = \boldsymbol{R}_{K} + \boldsymbol{S}_{K},$$

with:

$$E_{K} = e_{K} + \frac{1}{2} |\boldsymbol{u}_{K}|^{2},$$
$$E_{\sigma} = e_{\sigma} + \frac{1}{2} \boldsymbol{u}_{K} \cdot \boldsymbol{u}_{L},$$

$$(p\boldsymbol{u})_{K|L} = \frac{d_{K,\sigma}}{d_{\sigma}} p_K \boldsymbol{u}_L + \frac{d_{L,\sigma}}{d_{\sigma}} p_L \boldsymbol{u}_K.$$

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Pressure corr. schemes and all speed flows

A colocated scheme (6/7)

• S_K and total energy balance, without diffusion (continued):

Rest term:

$$R_{\mathcal{K}} = -\frac{|\mathcal{K}|}{2\delta t} \ \varrho_{\mathcal{K}}^* \ |\boldsymbol{u}_{\mathcal{K}} - \boldsymbol{u}_{\mathcal{K}}^*|^2.$$

For a regular function $(|\boldsymbol{u}_{K} - \boldsymbol{u}_{K}^{*}| \leq C \, \delta t)$:

$$\sum_{n}\sum_{K\in\mathcal{M}}\delta t|R_{K}|\leq C\delta t$$

but for a discontinuous function



=> choose $S_K = -R_K$.

A colocated scheme (7/7)

- Kinetic energy balance, S_K and total energy balance, with diffusion ($\varepsilon \neq 0$):
 - With a dissipation term:

$$R_{K} + = -\left[\sum_{\sigma=K|L} \varepsilon_{\sigma} \frac{|\sigma|}{d_{\sigma}} (\boldsymbol{u}_{K} - \boldsymbol{u}_{L})\right] \cdot \boldsymbol{u}_{K}$$

$$S_{K} + = \frac{1}{2} \sum_{\sigma=K|L} \varepsilon_{\sigma} \frac{|\sigma|}{d_{\sigma}} |\boldsymbol{u}_{K} - \boldsymbol{u}_{L}|^{2}.$$

Then:

$$R_{K}+S_{K}=\frac{1}{2}\sum_{\sigma=K|L}\varepsilon_{\sigma}\frac{|\sigma|}{d_{\sigma}}(\boldsymbol{u}_{K}-\boldsymbol{u}_{L})\cdot(\boldsymbol{u}_{K}+\boldsymbol{u}_{L}).$$

At the continuous level, the viscous term at the right-hand side of the total energy balance reads div $(\varepsilon \nabla^t \boldsymbol{u} \boldsymbol{u})$, so we need an approximation on the face of $(\nabla^t \boldsymbol{u} \boldsymbol{u}) \cdot \boldsymbol{n} = (\nabla \boldsymbol{u} \boldsymbol{n}) \cdot \boldsymbol{u} = \sum_{i=1}^{3} \boldsymbol{u}_i \nabla \boldsymbol{u}_i \cdot \boldsymbol{n} \dots$ which is what we get. $\boldsymbol{k}_{K} + S_{K}$ is conservative: conservation of $\int_{\Omega} \varrho \boldsymbol{E}$.

▶ Let $\varphi \in C_c^{\infty}(\Omega \times (0, T))$, and φ_K be an approximation of φ on K at the current time step. Then :

$$\sum_{n} \sum_{K \in \mathcal{M}} \delta t (R_{K} + S_{K}) \varphi_{K} = \frac{1}{2} \sum_{\sigma = K \mid L} \varepsilon_{\sigma} \frac{|\sigma|}{d_{\sigma}} (\boldsymbol{u}_{K} - \boldsymbol{u}_{L}) \cdot (\boldsymbol{u}_{K} + \boldsymbol{u}_{L}) (\varphi_{K} - \varphi_{L})$$
$$\leq C_{\varphi} \|\varepsilon\|_{L^{\infty}} \|\boldsymbol{u}\|_{L^{\infty}} \|\boldsymbol{u}\|_{BV}.$$

Pressure corr. schemes and all speed flows

A staggered scheme (1/2)



- > The velocity is now defined at the center of the faces.
- The approximation of \boldsymbol{u}_{σ} becomes natural.
- Up to this change, the mass mass balance and the left-hand side of the internal energy balance are left unchanged.
- Build mass fluxes at the dual faces in such a way that the mass balance is ensured on the diamond cells[†], and write the momentum balance equation on the diamond cells, following the same guidelines^{*} as for the colocated scheme.
 - †: L. Gastaldo, R. Herbin, W. Kheriji, JCL, FVCA 6.
 - *: convection term buit from the mass balance, pressure gradient built by duality.

A staggered scheme (2/2)

- A kinetic energy balance is still available, but is associated to faces, and can no more be combined to the internal energy equation (defined on primal meshes) to obtain a total energy balance equation.
- Strategy:

SK:

- 1- Suppose bounds and convergence for a sequence of discrete solutions, compatible with the regularity of the sought continuous solutions: control in BV and L^{∞} , convergence in L^{p} , for $p \geq 1$.
- 3- Let φ a regular function, (φ_{σ}) an interpolate on the faces and (φ_{K}) an interpolate on the cells, at the current time step. Multiply the kinetic energy balance by φ_{σ} , the internal energy balance by φ_{K} , sum over the time steps, *i*, σ and *K* and pass to the limit in the scheme.

 $\mathcal{S}_{\mathcal{K}}$ is chosen in such a way to recover, at the limit, the weak form of the total energy equation.

$$S_{K} = \sum_{\sigma \in \mathcal{E}(K)} \frac{|D_{K,\sigma}|}{\delta t} \varrho_{K}^{*} |\boldsymbol{u}_{\sigma} - \boldsymbol{u}_{\sigma}^{*}|^{2} + \sum_{\epsilon \subset K, \epsilon = \sigma | \sigma'} \varepsilon_{\epsilon} \frac{|\epsilon|}{d_{\epsilon}} |\boldsymbol{u}_{\sigma} - \boldsymbol{u}_{\sigma'}|^{2}.$$

An explicit time discretization

Scheme (time semi-discrete setting):

$$\begin{split} &\frac{1}{\delta t}(\varrho-\varrho^*) + \operatorname{div}(\varrho^*\boldsymbol{u}^*) = 0, \\ &\frac{1}{\delta t}(\varrho\boldsymbol{u}-\varrho^*\boldsymbol{u}^*) + \operatorname{div}(\varrho^*\boldsymbol{u}^*\otimes\boldsymbol{u}^*) - \operatorname{div}\boldsymbol{\tau}(\boldsymbol{u}^*) + \boldsymbol{\nabla}\boldsymbol{p}^* = 0, \\ &\frac{1}{\delta t}(\varrho\boldsymbol{e}-\varrho^*\boldsymbol{e}^*) + \operatorname{div}(\varrho^*\boldsymbol{e}^*\boldsymbol{u}^*) + \boldsymbol{p}^*\operatorname{div}\boldsymbol{u}^* = \boldsymbol{\tau}(\boldsymbol{u}^*): \boldsymbol{\nabla}\boldsymbol{u}^*, \\ &\boldsymbol{p} = (\gamma-1) \ \varrho\boldsymbol{e}. \end{split}$$

	S	к
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$$S_{K} = -\sum_{\sigma \in \mathcal{E}(K)} \frac{|D_{K,\sigma}|}{\delta t} \varrho_{K} |\boldsymbol{u}_{\sigma} - \boldsymbol{u}_{\sigma}^{*}|^{2} + \sum_{\epsilon \subset K, \ \epsilon = \sigma | \sigma'} \varepsilon_{\epsilon} \frac{|\epsilon|}{d_{\epsilon}} |\boldsymbol{u}_{\sigma}^{*} - \boldsymbol{u}_{\sigma'}^{*}|^{2}$$

A pressure correction scheme

Scheme (time semi-discrete setting):

$$\begin{aligned} \frac{1}{\delta t} (\varrho^* \tilde{\boldsymbol{u}} - \varrho^{**} \boldsymbol{u}^*) + \operatorname{div}(\varrho^* \tilde{\boldsymbol{u}} \otimes \boldsymbol{u}^*) - \operatorname{div} \boldsymbol{\tau}(\tilde{\boldsymbol{u}}) + \boldsymbol{\nabla} \boldsymbol{\rho}^* &= 0, \\ & \left| \begin{array}{c} \frac{\varrho^*}{\delta t} (\boldsymbol{u} - \tilde{\boldsymbol{u}}) + \boldsymbol{\nabla} (\boldsymbol{\rho} - \boldsymbol{\rho}^*) &= 0, \\ \frac{1}{\delta t} (\varrho - \varrho^*) + \operatorname{div}(\varrho \boldsymbol{u}) &= 0, \\ & \frac{1}{\delta t} (\varrho e - \varrho^* e^*) + \operatorname{div}(\varrho e \boldsymbol{u}) + \boldsymbol{\rho} \operatorname{div} \boldsymbol{u} &= \boldsymbol{\tau}(\tilde{\boldsymbol{u}}) : \boldsymbol{\nabla} \tilde{\boldsymbol{u}}, \\ & \boldsymbol{\rho} &= (\gamma - 1) \ \varrho e. \end{aligned} \end{aligned} \right.$$

► S_K:

$$S_{K} = \sum_{\sigma \in \mathcal{E}(K)} \frac{|D_{K,\sigma}|}{\delta t} \varrho_{K}^{*} |\tilde{\boldsymbol{u}}_{\sigma} - \boldsymbol{u}_{\sigma}^{*}|^{2} + \sum_{\epsilon \subset K, \ \epsilon = \sigma | \sigma'} \varepsilon_{\epsilon} \frac{|\epsilon|}{d_{\epsilon}} |\tilde{\boldsymbol{u}}_{\sigma} - \tilde{\boldsymbol{u}}_{\sigma'}|^{2}.$$

• If a pressure renormalization step is added, this scheme is unconditionnally stable $(\varrho > 0, e > 0, \varrho$ and ϱE controlled in $L^{\infty}(0, T; L^{1}))$. In addition, the time splitting yields a control on $\delta t \nabla p$ in $L^{\infty}(0, T; L^{2})$.

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Numerical tests

A Riemann Problem

[P. Woodward, P. Collela, JCP 1984]
 [E. Toro, *Riemann solvers and numerical methods for fluid dynamics*, third edition, test 5 of chapter 4].

Two shocks travelling to the right, contact discontinuity.

- Computation performed with the upwind explicit scheme.
- $\delta t = h/50$, so a cfl number close to 1/2.
- An additional diffusion term is added in the momentum balance equation, in the range of *Quh/2*.



Numerical tests

A Riemann Problem



Numerical tests

A Riemann Problem



- Difference between the numerical and analytical solution (L¹ norm), as a function of the time and space step (cfl ≈ 0.4).
- First order convergence for the quantities which remain constant through the contact discontinuity (u, p).

Convergence as $h^{1/2}$ for ρ .

A Riemann Problem



Right $S_K = 0$.

A Riemann Problem



Right: no additional diffusion.

Conclusion

Conclusion

- A class of naive schemes for Euler equations:
 - staggered mesh,
 - upwinding with respect to the (material) velocity, centered approximation of the pressure gradient,
 - ▶ total energy equation \hookrightarrow internal energy equation + source term,
 - ▶ a reasonably decoupled (?) unconditionally stable time discretization (?).
- ► Convergence ?
 - 1. estimates: $\rho > 0$, e > 0, ρ and ρE controlled in $L^{\infty}(0, T; L^{1})$, entropy ?
 - 2. Compactness: far from being sufficient ! (no control on the translations)
 - 3. Passage to the limit in the scheme: OK.
- Tests under progress.
- ► Further developments: less diffusive versions (entropy viscosity technique ?)