

B. Després LJLL-Paris VI+CEA

Thanks to PhD: Mazeran, Kluth, Franck, CEA: Delpino, Labourasse, Carre, Buet, ..., and all

and all colleagues along these years. Numerical methods for FCI Part II: Hydrodynamics

> B. Després LJLL-Paris VI+CEA

Thanks to PhD: Mazeran, Kluth, Franck, CEA: Delpino, Labourasse, Carre, Buet, ..., and all colleagues along these years.

3

<ロト <回ト < 三ト < 三ト



FCI scenario

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis



Irradiation Implosion Ignition Combustion

Hydrodynamic is dominant in the implosion stage

Numerical methods for FCI Part II: Hydrodynamics

1



DT capsule in a gold cylinder, heated by laser beams Credit CEA/DAM/DIF

Introduction

PDEs

Schemes-

Numerical results

Numerical analysis





∃ ► < ∃ ►</p>

The radiation push is not perfectly symetric

Numerical methods for FCI Part II: Hydrodynamics

Э



Why Lagrangian scheme for compressible flows?

Introduction

PDEs

- Schemesconstruction
- Numerical results
- Numerical analysis

- Lagrangian methods are written in the fluid frame
- easy discretization of free boundaries (external and internal),
- naturally adapted for multimaterial flows,
- very good accuracy for transport dominated flows



∃ ► < ∃ ►</p>



3D examples

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis









Perturbation of a basic flow

<ロト <回ト < 三ト < 三ト

Introduction

PDEs

- Schemesconstruction
- Numerical results

Numerical analysis ICF flows are very sensitive to hydrodynamic perturbation. That is a even very small initial pertubation may have a dramatic influence on the solution. The reason is that ICF flows are quite close to instability, so that the growth rate of the perturbations may be large. Numerical methods are very useful to quantify the influence these perturbations. Here we illustrate with the result of a very simple numerical simulation done by E. Franck during his Master 2.



The mesh at t = 0 is displayed on the left. The perturbation is a n = 16 mode. On the right the result at time $t_f = 10^{-9}s$. On this simulation the growth rate of the perturbation is reasonnable.

Lagrangian methods are essential for such simulations.

Eulerian methods on Cartesian meshes are less efficient.



Plan

Introduction

PDEs

Schemes-

construction

Numerical results

Numerical analysis

- Partial Differential Equations
- Meshes and schemes
- Numerical analysis : stability, CFL, convergence (new)
- $T_i T_e$ discretization
- Extension to radiation.
- Development of Hele-Shaw models (for stability of ICF flows, with H. Egly and R. Sentis).

1

《曰》《圖》《注》《注》

JL

Euler equations

The Euler equation for compressible gas dynamics are

Introduction

PDEs

Schemes-

construction

Numerical results

Numerical analysis $\left\{ \begin{array}{l} \partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0, \\ \partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla \rho = 0, \\ \partial_t (\rho e) + \nabla \cdot (\rho \mathbf{u} e + \rho \mathbf{u}) = 0, \\ \partial_t (\rho S) + \nabla \cdot (\rho \mathbf{u} S) \ge 0. \end{array} \right.$

The density is $\rho > 0$. The velocity is $\mathbf{u} \in \mathbb{R}^d$. The density of total energy is $e = \varepsilon + \frac{1}{2} |\mathbf{u}|^2$. Possible EOS

$$p = (\gamma - 1)\rho\varepsilon$$
, $p = (\gamma - 1)\rho\varepsilon - \gamma p_0$, $p = tabulated$, $p = analytic$.

Assumption : there exists a temperature T > 0 such that

$$TdS = d\varepsilon + pd\tau, \quad \tau = \frac{1}{\rho}.$$

The pressure $p = p(\tau, \varepsilon)$ is provided by the equation of state.

The entropy inequality selects the entropy solutions of the Euler system.

For a perfect gas EOS, $\varepsilon = C_v T$ and $S = \log(\varepsilon \tau^{\gamma - 1})$.

Э

イロト イヨト イヨト イヨト

Quasi-Lagrange in 2D

《口》 《圖》 《臣》 《臣》



Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis It writes

1

$$\begin{cases} \rho D_t \tau - \nabla \cdot \mathbf{u} = 0, \\ \rho D_t \mathbf{u} + \nabla p = 0, \\ \rho D_t e + \nabla \cdot (p\mathbf{u}) = 0, \end{cases}$$

where the material derivative is
$$D_t=\partial_t+{f u}\cdot
abla$$
 .
Or also with an artificial viscosity q

$$\begin{cases} \rho D_t \tau - \nabla \cdot \mathbf{u} = 0, \\ \rho D_t \mathbf{u} + \nabla (p+q) = 0, \\ \rho D_t \varepsilon + (p+q) \nabla \cdot \mathbf{u} = 0. \end{cases}$$

By construction

$$\rho T d_t S = \rho D_t \varepsilon + p \rho D_t \tau = -q \nabla \cdot \mathbf{u} \ge 0$$

A possible artificial viscosity is $q = C\Delta x \max(0, -\nabla \cdot \mathbf{u}) \ge 0$. I will not discuss these methods which are non conservative. The seminal idea's comes from Von Neumann.



Reminder

• A non linear system of conservation laws with an entropy writes

$$\partial_t U + \partial_x f(U) + \partial_y g(U) = 0.$$

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis • Assume the system is endowed with a strictly convex entropy $\widehat{S}(U) \in \mathbb{R}$: smooth solutions satisfy $\partial_t \widehat{S}(U) + \partial_x F(U) + \partial_y G(U) = 0$.

• Then the system is hyperbolic, which implies stability around constant, and well posedness of the Cauchy problem for smooth initial data in finite time 0 < t < T.

• Discontinuous solutions satisfy the Rankine Hugoniot relation

$$-\sigma \left(U_R - U_L\right) + n_x \left(f(U_R) - f(U_L)\right) n_y \left(g(U_R) - g(U_L)\right) = 0$$

and the entropy inequality

$$-\sigma\left(\widehat{S}(U_R)-\widehat{S}(U_L)\right)+n_x\left(F(U_R)-F(U_L)\right)n_y\left(G(U_R)-G(U_L)\right)\geq 0.$$

Problem : the Quasi-Lagrange formulations are not conservative.

Question : how to write pure conservative Lagrange PDE's? cf Godlewski-Raviart, Serre, ...

Question : how about hyperbolicity for Lagrangian systems?



<ロ> (四) (四) (三) (三) (三) (三)



Introduction

$$x = (x, y)$$
 and $X = (X, Y)$.



Schemesconstruction

Numerical results

Numerical analysis Let us consider the Euler-to-Lagrange change of frame defined by

 $\partial_t \mathbf{x}(\mathbf{X}, t) = u(\mathbf{x}(\mathbf{X}, t), t)$ with initialization $\mathbf{x}(\mathbf{X}, 0) = \mathbf{X}$.





We need a tool to rewrite the equations in the X frame.

Piola's transformations

イロト イヨト イヨト イヨト

PDEs

Schemesconstruction

Numerical results

Numerical analysis **Rule 1** A smooth change of variable $\mathbf{x} \mapsto \mathbf{X}(\mathbf{x})$ is such that $\mathbf{n}d\sigma = \operatorname{cof}(\nabla_{\mathbf{X}}\mathbf{x})\mathbf{n}_{\mathbf{X}}d\sigma_{\mathbf{X}}$. where $\operatorname{cof}(M) \in \mathbb{R}^{d \times d}$ is the comatrix of M.

Rule 2 A system of conservation laws $\nabla_x F(U) = 0$ written in the eulerian variable is transformed in a lagrangian system written with the **X** variable

$$\nabla_X \cdot [F(U) \operatorname{cof} (\nabla_X \mathbf{x})] = 0.$$

This is a consequence of rule 1.

Rule 3 One must not forget the Piola's identity

$$\nabla_X . \operatorname{cof} (\nabla_X \mathbf{x}) = 0.$$

A reason is that the system contains a new unknown cof ($\nabla_X x$). Therefore we need a new equation to close the system..

Э





PDEs in 1D

We consider the change of coordinates $(x, t) \mapsto X, t$ in \mathbb{R}^2 . The gradient of the space-time transformation is $\begin{pmatrix} 1 & 0 \\ u & J \end{pmatrix}$ with the Jacobian $J = \frac{\partial x}{\partial X}$. The comatrix is $\operatorname{cof} = \begin{pmatrix} J & -u \\ 0 & 1 \end{pmatrix}$. The Lagrangian system is

Introduction

PDEs

$$\nabla_{X,t} \cdot \left[\begin{pmatrix} \rho & \rho u \\ \rho u & \rho u^2 + p \\ \rho e & \rho u e + p u \end{pmatrix} \begin{pmatrix} J & -u \\ 0 & 1 \end{pmatrix} \right] = \partial_t \begin{pmatrix} \rho J \\ \rho J u \\ \rho J e \end{pmatrix} + \partial_X \begin{pmatrix} 0 \\ p \\ p u \end{pmatrix} = 0$$

Numerical

Numerical analysis The Piola identity writes

 $\partial_t J - \partial_X u = 0.$

It is usual to define the mass variable

$$dm = \rho(x, t)dx = \rho(X, 0)dX$$

which is independent of the time, to eliminate the density

 $\rho J = \rho(X, 0)$

and to get the system of conservation laws in the mass variable

$$\begin{cases} \partial_t \tau - \partial_m u = 0, \\ \partial_t u + \partial_m p = 0, \\ \partial_t e + \partial_m (pu) = 0. \end{cases}$$

Notice that $\rho > 0$ is necessary for the validity of the transformation $rac{1}{2}$ $rac{$

Numerical methods for FCI Part II: Hydrodynamics



$$\begin{split} B &= \partial_X y, \ L &= \partial_Y x \ \text{and} \ M &= \partial_Y y. \\ \text{The algebra of the Euler-Lagrange transformation is as follows. The space-time deformation gradient is$$
 $<math display="block">\begin{pmatrix} 1 & 0 & 0 \\ u & A & L \\ v & B & M \end{pmatrix}. \ \text{The comatrix is cof} = \begin{pmatrix} J & -uM + vL & uB - vA \\ 0 & M & -B \\ 0 & -L & A \end{pmatrix} \text{ where the space Jacobian} \\ \text{is } J &= AM - BL. \ \text{The product of matrices is} \\ \begin{pmatrix} \rho & \rho u & \rho v \\ \rho u & \rho u^2 + \rho & \rho uv \\ \rho v & \rho uv & \rho v^2 + \rho \\ o e & oue + pu & ove + pv \end{pmatrix} \text{cof} = \begin{pmatrix} \rho J & 0 & 0 \\ \rho uJ & pM & -\rho B \\ \rho vJ & -\rho L & \rho A \\ \rho eJ & p uM - pvL & -puB + pvA \end{pmatrix}. \end{split}$

Let us define for convenience the components of the deformation gradient $\mathbf{F} = \nabla_{\mathbf{X}} \mathbf{x}$ as $A = \partial_{X} x_{i}$

Numerical analysis

Numerical

PDEs

So the Eulerian system is transformed into the Lagrangian system

$$\begin{cases} \partial_t(\rho J) = 0, \\ \partial_t(\rho J u) + \partial_X(\rho M) + \partial_Y(-\rho B) = 0, \\ \partial_t(\rho J v) + \partial_X(-\rho L) + \partial_Y(\rho A) = 0, \\ \partial_t(\rho J e) + \partial_X(p u M - p v L) + \partial_Y(p v A - p u B) = 0. \end{cases}$$

The Piola's identities writes

$$\begin{cases} \partial_t J - \partial_X (uM - vL) - \partial_Y (vA - uB) = 0, \\ \partial_X M - \partial_Y B = 0, \\ -\partial_X L + \partial_Y A = 0. \end{cases}$$

It is not a closed system of conservation laws.

Numerical methods for FCI Part II: Hydrodynamics

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □

Hui's system



• The Hui's system is closed

Introduction

PDEs

Schemes-

Numerical

Numerical

analysis

- $\left\{ \begin{array}{l} \partial_t(\rho J) = 0, \\ \partial_t(\rho Ju) + \partial_X(\rho M) + \partial_Y(-\rho B) = 0, \\ \partial_t(\rho Jv) + \partial_X(-\rho L) + \partial_Y(\rho A) = 0, \\ \partial_t(\rho Je) + \partial_X(\mu M \rho vL) + \partial_Y(\rho vA \rho uB) = 0, \\ \partial_t A = \partial_X u, \\ \partial_t B = \partial_X v, \\ \partial_t B = \partial_Y v, \\ \partial_t L = \partial_V u, \\ \partial_t M = \partial_Y v, \\ J = AM BL. \end{array} \right.$
- · A second system is more concerned with the formal symetry of the fluxes

$$\left\{ \begin{array}{ll} \rho_0 \partial_t \tau - \partial_X (uM - vL) - \partial_Y (vA - uB) = 0, & \rho_0 = \rho J, \quad \tau = \frac{1}{\rho}, \\ \rho_0 \partial_t u + \partial_X (pM) + \partial_Y (-\rho B) = 0, \\ \rho_0 \partial_t v + \partial_X (-\rho L) + \partial_Y (pA) = 0, \\ \rho_0 \partial_t e + \partial_X (puM - pvL) + \partial_Y (pvA - puB) = 0. \end{array} \right.$$

The symetry is related to the fact that (M, L) appears only in the X derivative, and (A, B) is the Y derivative.

1



A potential closed formulation

・ロト ・回ト ・ヨト ・ヨト

The third formulation makes use of the Piola-Kirkhoff tensor (with G. Kluth). Since $\rho J = \rho_0$ then $\tau = \frac{AM - BL}{\rho_0}$ and therefore

Introduction

PDEs

 $\sigma^{PK} = \rho_0 \nabla_{\mathbf{F}|S} \varepsilon = \left(\rho_0 \frac{\partial \varepsilon}{\partial \tau|S} \right) \nabla_{\mathbf{F}} \tau = -p \left(\begin{array}{cc} M & -B \\ -L & A \end{array} \right).$

Schemes-

construction

Numerical results

Numerical analysis It writes in a compact form

$$\left\{ \begin{array}{ll} \partial_t \mathbf{F} = \nabla_{\mathbf{X}} \mathbf{u}, \\ \rho_0 \partial_t \mathbf{u} = \nabla_{\mathbf{X}} \cdot \sigma^{PK}, \\ \rho_0 \partial_t e = \nabla_{\mathbf{X}} \cdot (\mathbf{u}^t \sigma^{PK}). \end{array} \right.$$

Entropy : One has from the fundamental principle of thermodynamics $\rho_0 \partial_t \varepsilon = \rho_0 \left(T \partial_t S + \nabla_{\mathsf{F}|S} \varepsilon : \partial_t \mathsf{F} \right)$. Therefore

$$\rho_0 T \partial_t S = -\sigma^{PK} : \partial_t \mathbf{F} + \rho_0 \partial_t e - \mathbf{u} \cdot \rho_0 \partial_t \mathbf{u}$$
$$= -\sigma^{PK} : \nabla_{\mathbf{X}} \mathbf{u} - \mathbf{u} \cdot \nabla_{\mathbf{X}} \cdot \sigma^{PK} + \nabla_{\mathbf{X}} \cdot (\mathbf{u}^t \sigma^{PK}) = 0.$$

For shock solutions

 $\partial_t S \ge 0$

in the sense of distributions.

Mass variables in 2D

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □

Introduction Assumption : there exists two independent variables (α, β) such that PDEs Schemesconstruction Numerical results Numerical analysis and $\partial_{\beta} = \frac{\partial X}{\partial \beta} \partial_{X} + \frac{\partial Y}{\partial \beta} \partial_{Y} = \frac{1}{\rho_{0}} \partial_{X} \Longrightarrow \frac{1}{\rho_{0}} = \frac{\partial X}{\partial \alpha} \text{ and } 0 = \frac{\partial Y}{\partial \alpha}$

In this case $\frac{\partial \rho^{-1}}{\partial_{\beta}} = \frac{\partial^2 \chi}{\partial \alpha \partial \beta} = 0$ and $\frac{\partial \rho^{-1}}{\partial_{\alpha}} = \frac{\partial^2 \gamma}{\partial \alpha \partial \beta} = 0$. So the density ρ is a constant.

It is not possible to define simple mass variables as in dimension one.

Numerical methods for FCI Part II: Hydrodynamics



Hyperbolicity

• In dimension one, the size of the lagrangian system is s = 3. One checks easily that $-S = -\log(\varepsilon \tau^{\gamma-1})$ is strictly convex with respect to τ , u, e. Therefore the lagrangian system is hyperbolic in 1D.

In dimension two, the situation is less evident because the algebra is tricky and the interpretation of the
results may depend on particular version of the lagrangian chosen for the analysis. In all cases the result is
that lagrangian systems in dimension greater or equal to two are weakly hyperbolic. Perhaps more important
is to understand what are the consequences of weak hyperbolicity on the one hand for the solution of the
Cauchy problem in dimension two and more, and on the other hand for numerical simulations.

• The Cauchy problem of a system of conservation which is only weakly hyperbolic suffers of a loss of derivatives. That is one is able to show stability inequalities in ad-hoc functional spaces like

 $\|U(t)\|_{H^m} \le C \|U(0)\|_{H^{m+p}}, \qquad 0 < t < T.$

The integer p > 0 measures the number of derivatives which are loosed by the solution of Cauchy problem. Such a phenomenon is characteristic of a weakly hyperbolic system.

• Let us study a particular Cauchy problem for any lagrangian systems in dimension two. The initial data are

p(X, Y, 0) is a constant, and u(X, Y, 0) = w(Y), v(X, Y, 0) = 0.

The physical solution is of course a pure shear flow

$$x(X, Y, t) = X + tw(Y) \text{ and } y(X, Y, t) = Y.$$

Therefore

$$\mathbf{F}(t) = \begin{pmatrix} 1 & tw'(Y) \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 & t\partial_Y u(0) \\ 0 & 1 \end{pmatrix}$$

So the deformation gradient is a function of the Y derivative of the velocity at time t = 0. In consequence the Cauchy problem suffers for the loss of at least one derivative. $\langle \Box \rangle = \langle \Box \rangle = \langle$

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis



Context

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis

- Historical topic : Von Neumann-Richtmyer VNR scheme, Godunov Gaia scheme (Godunov-Lagrange)
- Other active researchers on Lagrangian numerical methods : R. Loubere, G. Scovazzi (Sandia), M. Shaskov (T7), ..., C.W. Shu, ...

• CELIA group : Multi-scale Godunov-type method for bf cell-centered discrete Lagrangian hydrodynamics JCP 2009, Maire-Nkonga

• <u>CEA</u> group : A cell-centered Lagrangian hydrodynamics scheme on general unstructured meshes in arbitrary dimension JCP 2009, Carré, Del Pino, D. et Labourasse

Э

イロト イヨト イヨト イヨト

In 1D



In dimension one, it is sufficient to rely on the theory of the solutions to the Riemann problem in order to establish a rigorous and efficient basis for the development of numerical schemes. The basic scheme that one obtains with this method writes

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis $\begin{cases} \frac{M_j}{\Delta t} (\tau_j^{n+1} - \tau_j^n) - u_{j+\frac{1}{2}}^* + u_{j-\frac{1}{2}}^* = 0, \\ \frac{M_j}{\Delta t} (u_j^{n+1} - u_j^n) + p_{j+\frac{1}{2}}^* - p_{j-\frac{1}{2}}^* = 0, \\ \frac{M_j}{\Delta t} (e_j^{n+1} - e_j^n) + p_{j+\frac{1}{2}}^* u_{j+\frac{1}{2}}^* - p_{j-\frac{1}{2}}^* u_{j-\frac{1}{2}}^* = 0. \end{cases}$

where the fluxes are defined by an approximation of the Riemann problem. For example

$$\left\{ \begin{array}{l} u_{j+\frac{1}{2}}^{*} = \frac{1}{2}(u_{j}^{n} + u_{j+1}^{n}) + \frac{1}{2\rho c}(p_{j}^{n} - p_{j+1}^{n}) \\ p_{j+\frac{1}{2}}^{*} = \frac{1}{2}(p_{j}^{n} + p_{j+1}^{n}) + \frac{\rho c}{2}(u_{j}^{n} - u_{j+1}^{n}). \end{array} \right.$$

The local acoustic ρc impedance is povided by an approximated formula : for example by $(\rho c)_{j+\frac{1}{2}} = \frac{1}{2} \left[(\rho c)_{j+1}^n + (\rho c)_{j+1}^n \right]$. More robust and accurate formulas for the local impedance are possible. The mass of cell number j is

$$M_j = \rho_j^0 \Delta x_j^0 = \rho_j^n \Delta x_j^n.$$

The displacement of the cell is defined by

$$x_{j+\frac{1}{2}}^{n+1} = x_{j+\frac{1}{2}}^{n} + \Delta t u_{j+\frac{1}{2}}^{*}.$$

It is a enlightening classroom exercise to show that all these formulas are compatible ... , a 😑 , 🚊 🛶 🖓 🖉



Exercise + correction

《曰》《聞》《臣》《臣》



PDEs

Schemesconstruction

Numerical results

Numerical analysis We want by induction on n to show the compatibility of the discrete equations

$$\begin{cases} \frac{M_j}{\Delta t} (\tau_j^{n+1} - \tau_j^n) - u_{j+\frac{1}{2}}^* + u_{j-\frac{1}{2}}^* = 0, \\ M_j = \rho_j^n \Delta x_j^n, \\ x_{j+\frac{1}{2}}^{n+1} = x_{j+\frac{1}{2}}^n + \Delta t u_{j+\frac{1}{2}}^*. \end{cases}$$

The starting point is
$$M_j^n = \rho_j^n \Delta x_j^n = \rho_j^n \left(x_{j+\frac{1}{2}}^n - x_{j-\frac{1}{2}}^n \right)$$
. So

$$\frac{\rho_{j}^{n}\Delta x_{j}^{n}}{\rho_{j}^{n+1}} = \Delta x_{j}^{n} + \Delta t \left(u_{j+\frac{1}{2}}^{*} - u_{j-\frac{1}{2}}^{*} \right) = \Delta x_{j}^{n+1}.$$

CQFD.

Implementation

$$\begin{cases} \frac{M_j}{\Delta t} (u_j^{n+1} - u_j^n) + p_{j+\frac{1}{2}}^* - p_{j-\frac{1}{2}}^* = 0, \\ \frac{M_j}{\Delta t} (e_j^{n+1} - e_j^n) + p_{j+\frac{1}{2}}^* u_{j+\frac{1}{2}}^* - p_{j-\frac{1}{2}}^* u_{j-\frac{1}{2}}^* = 0. \end{cases}$$

At the same time move the mesh

$$x_{j+\frac{1}{2}}^{n+1} = x_{j+\frac{1}{2}}^{n} + \Delta t u_{j+\frac{1}{2}}^{*},$$

and recompue the density

$$\rho_j^{n+1} = \frac{M_j}{\Delta x_j^{n+1}}.$$

Numerical methods for FCI Part II: Hydrodynamics



Entropy :
$$S'_j(t) \ge 0$$

イロト イヨト イヨト イヨト



Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis The fundamental principle of thermodynamics $TdS = d\varepsilon + pd\tau$ implies

$$M_j T_j(t) S'_j(t) = M_j \left(\varepsilon'_j(t) + p_j \tau'_j(t) \right) = M_j e'_j(t) - M_j u_j u'_j(t) + M_j p_j \tau'_j(t)$$

 $u_{j+\frac{1}{2}}^{*}+u_{j-\frac{1}{2}}^{*}\left\{\begin{array}{l} M_{j}\tau_{j}'(t)-u_{j+\frac{1}{2}}^{*}+u_{j-\frac{1}{2}}^{*}=0,\\ M_{j}u_{j}'(t)+p_{j+\frac{1}{2}}^{*}-p_{j-\frac{1}{2}}^{*}=0,\\ M_{j}e_{j}'(t)+p_{j+\frac{1}{2}}^{*}u_{j+\frac{1}{2}}^{*}-p_{j-\frac{1}{2}}^{*}u_{j-\frac{1}{2}}^{*}=0.\end{array}\right.$

$$= -\left(p_{j+\frac{1}{2}}^{*}u_{j+\frac{1}{2}}^{*} - p_{j-\frac{1}{2}}^{*}u_{j-\frac{1}{2}}^{*}\right) + u_{j}\left(p_{j+\frac{1}{2}}^{*} - p_{j-\frac{1}{2}}^{*}\right) + \rho_{j}\left(u_{j+\frac{1}{2}}^{*} - u_{j-\frac{1}{2}}^{*}\right) - (0 = (\rho_{j}u_{j} - \rho_{j}u_{j}))$$

$$= -\left(p_{j+\frac{1}{2}}^{*} - \rho_{j}\right)\left(u_{j+\frac{1}{2}}^{*} - u_{j}\right) + \left(p_{j-\frac{1}{2}}^{*} - \rho_{j}\right)\left(u_{j-\frac{1}{2}}^{*} - u_{j}\right)$$

The Riemann solver is the solution of the system

$$\begin{cases} p_{j+\frac{1}{2}}^* - p_j + (\rho c)_{j+\frac{1}{2}} \left(u_{j+\frac{1}{2}}^* - u_j \right) = 0, \\ p_{j+\frac{1}{2}}^* - p_{j+1} - (\rho c)_{j+\frac{1}{2}} \left(u_{j+\frac{1}{2}}^* - u_j \right) = 0 \end{cases}$$

Therefore $S'_i(t) \ge 0$.

For design and justification, the equations for the Riemann solver are more important than its solution

Э



Schemesconstruction Numerical results Numerical analysis

Why the mesh is stable

For simplicity we consider the semi-discrete case (continuous in time scheme) and a perfect gas equation of state with $\gamma = 2$ $S = \log(\varepsilon \tau)$.

FFCW

$$C = \min_{j} \left(\varepsilon_{j}^{0} \tau_{j}^{0} \right), \quad F \leq \frac{\sum_{\rho} M_{\rho} e_{\rho}}{M_{j}} \leq \frac{E^{0}}{\min_{j} M_{j}}, \quad W \leq \frac{\sum_{\rho} M_{\rho} \tau_{\rho}^{0}}{M_{j}} = \frac{V^{0}}{\min_{j} M_{j}}$$

Therefore

$$au_j(t) > 0 \Longrightarrow \Delta x_j(t) = rac{M_j}{ au_j(t)} > 0.$$

It shows a very strong coupling of thermodynamics and mesh stability. Ξ > Ξ \mathcal{O}

Numerical methods for FCI Part II: Hydrodynamics

Moving meshes in ND



Schemesconstruction

Numerical

analysis



j is the index of the cell, k denotes the time step. V_i^k is the volume at time step k.

We assume that a formula holds that gives the volume in function of the vertices

 $(\mathbf{x}_1, \cdots, \mathbf{x}_r, \cdots) \mapsto V_j(\mathbf{x}_1, \cdots, \mathbf{x}_r, \cdots).$

This is the key assumption.

For example such a formula holds for the isoparametric element $(=Q^1)$ even if the faces are **warped**. Let us denote $\mathbf{x}^k = (\mathbf{x}_1^k, \cdots, \mathbf{x}_r^k, \cdots)$ the collection of all vertices of the mesh. A fundamental discrete object defined even for cells with warped faces is

$$\mathbf{C}_{jr} = \nabla_{\mathbf{x}_{r}} V_{j} = \begin{pmatrix} \frac{\partial}{\partial \mathbf{x}_{r,1}} V_{j} \\ \cdots \\ \frac{\partial}{\partial \mathbf{x}_{r,d}} V_{j} \end{pmatrix} \in \mathbb{R}^{d}.$$



What is C_{jr} ?

• 1D :
$$r = j + \frac{1}{2}$$
 is the vertex between j and $j + 1$. Then $V_j = x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}}$.
So $C_{j,j+\frac{1}{2}} = 1$ and $C_{j,j-\frac{1}{2}} = -1$.

Introduction

PDEs

• 2D:
$$V_j = \sum_r \frac{1}{2} (x_r y_{r+1} - y_r x_{r+1}) \Longrightarrow C_{jr} = \frac{1}{2} \begin{pmatrix} -y_{r-1} + y_{r+1} \\ x_{r-1} - x_{r+1} \end{pmatrix}$$

Schemesconstruction

Numerical results

Numerical analysis



Answer: $C_{jr} = l_{jr} n_{jr}$ is a corner generalization of the face quantity $l_j n_f$.

1

< 日 > < 四 > < 三 > < 三 > < 三 > <



 \mathbf{C}_{jr} in 3D

Tetrahedrons

PDEs

Schemesconstruction

Numerical results

Numerical analysis



$$\mathbf{C}_{j1} = \frac{1}{6} \left(\left| \begin{array}{cccc} y_2 & y_3 & y_4 \\ z_2 & z_3 & z_4 \\ 1 & 1 & 1 \end{array} \right|, - \left| \begin{array}{cccc} x_2 & x_3 & x_4 \\ z_2 & z_3 & z_4 \\ 1 & 1 & 1 \end{array} \right|, \left| \begin{array}{cccc} x_2 & x_3 & x_4 \\ y_2 & y_3 & y_4 \\ 1 & 1 & 1 \end{array} \right| \right)^t = -\frac{1}{3} \left| f_{234} \right| \mathbf{n}_{234}.$$

• Hexahedrons

$$\mathbf{C}_1 = \nabla_{\mathbf{x}_1} V = \frac{1}{12} \sum_{r=2}^8 \sum_{s=r+1}^8 \mathbf{x}_r \wedge \mathbf{x}_s, \qquad \mathbf{x}_1, \mathbf{x}_r, \mathbf{x}_s \in \mathsf{same face}.$$

Warped faces are allowed.

1

▲ロト ▲圖ト ▲注ト ▲注ト



One has

$$\frac{d}{dt}V_j = \left(\nabla_{\mathbf{x}}V_j, \mathbf{x}'\right) = \sum_r \left(\mathbf{C}_{jr}, \mathbf{u}_r\right).$$

Introduction

PDEs

By homogeneity :

$$V_j = \frac{1}{d} \left(\nabla_{\mathbf{x}} V_j, \mathbf{x} \right) = \frac{1}{d} \sum_r \left(\mathbf{C}_{jr}, \mathbf{x}_r \right).$$

 $\sum C_{jr}=0.$

Schemesconstruction

Numerical results

Numerical analysis • For all cell *j* one has

• For all interior vertices xr

 $\sum_{j} \mathbf{C}_{jr} = \mathbf{0}.$

The mass of a Lagrangian cell is constant in time : $V_j(\mathbf{x}(t))\rho_j(t) = M_j$ is independent of the time t. So

$$M_j \tau_j'(t) = \frac{d}{dt} V_j(\mathbf{x}(t)) = \sum_r \left(\mathsf{C}_{jr}, \mathbf{u}_r \right), \quad \tau_j = \frac{1}{\rho_j}.$$

The hydrodynamics equations imply $\rho \frac{d}{dt} \tau = \nabla \cdot \mathbf{u}$. It means that $\sum_r (\mathbf{C}_{jr}, \mathbf{u}_r)$ is an approximation in the Finite Volume sense of $\nabla \cdot \mathbf{u}$ over the moving cell j

$$\int_{V_j} \nabla \cdot \mathbf{u} \, d\mathbf{x} = \int_{\partial V_j} \left(\mathbf{u}, \mathbf{n} \right) \, d\sigma \approx \sum_r \left(\mathbf{C}_{jr}, \mathbf{u}_r \right) \, .$$

In some the Finite Volume scheme is corner based.

Numerical methods for FCI Part II: Hydrodynamics

Properties

p. 27 / 41

1



The nodal solver for cell centered data $(\rho_j, \mathbf{u}_j, \cdots)$

• The first formula expresses that the sum of all forces around the vertex \mathbf{x}_r is zero

Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis $\sum_{i} \mathbf{C}_{jr} p_{jr} = 0.$



This natural formula, also used for staggered schemes, enforces the conservation of momentum.

• The second formula is a multidimensional generalization of a first-order Riemann solver

$$p_{jr} - p_j + \rho_j c_j \left(\mathbf{u}_r - \mathbf{u}_j, \mathbf{n}_{jr} \right) = 0, \qquad \mathbf{n}_{jr} = \frac{\mathbf{C}_{jr}}{|\mathbf{C}_{jr}|}, \quad |\mathbf{n}_{jr}| = 1.$$



This the magic formula for those not acquainted wit acoustic Riemann solvers.

Solution



One can eliminate the pressures and gets a linear system : $A_ru_r=b_r.$ The unknown vector is the node velocity $u_r\in\mathbb{R}^d.$ The matrix is

$$\mathbf{A}_{r} = \sum_{j} \rho_{j} c_{j} \frac{\mathbf{C}_{jr} \otimes \mathbf{C}_{jr}}{|\mathbf{C}_{jr}|} \in \mathbb{R}^{d \times d} = \mathbf{A}_{r}^{t} > 0.$$

Introduction

The right hand side is

$$\mathbf{b}_{r} = \sum_{j} \mathbf{C}_{jr} \rho_{j} + \sum_{j} \rho_{j} c_{j} \frac{\mathbf{C}_{jr} \otimes \mathbf{C}_{jr}}{|\mathbf{C}_{jr}|} \mathbf{u}_{j} \in \mathbb{R}^{d}.$$

construction Numerical results

Numerical analysis The solution of the linear system is $\mathbf{u}_r = \mathbf{A}_r^{-1} \mathbf{b}_r$. Once the nodal velocities \mathbf{u}_r have been calculated, one computes the nodal pressures $\rho_{jr} \ \rho_{jr} = \rho_j + \rho_j c_j \ (\mathbf{u}_r - \mathbf{u}_j, \mathbf{n}_{jr})$.

- 1) Compute the geometrical vectors \mathbf{C}_{ir}^k for all j, r.
- 2) Determine the nodal velocities \mathbf{u}_r^k and the nodal pressures p_{ir}^k using the nodal solver.
- 3) Update the momentum

$$M_j \frac{\mathbf{u}_j^{k+1} - \mathbf{u}_j^k}{\Delta t} = -\sum_r \mathbf{C}_{jr}^k p_{jr}^k.$$

The total energy is updated with

$$M_j \frac{e_j^{k+1} - e_j^k}{\Delta t} = -\sum_r \left(\mathbf{C}_{jr}^k, \mathbf{u}_r^k\right) p_{jr}^k.$$

(日) (日) (日)

Then the vertices are moved x_r^{k+1} = x_r^k + ∆t u_r^k.
 Update the new density in the cell ρ_i^{k+1} = M_i/(k+1).

Numerical methods for FCI Part II: Hydrodynamics



Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis Finite Volume Lagrangian cell-centered schemes are possible, but at the price of changing the notion of what is a Finite Volume flux.

Consequence : The structure of the code is slightly different.



The Kidder test problem

A portion of a shell $r_i = 0.9 \le r \le 1 = r_e$ is filled with a perfect gas. The adiabatic constant of the gas is $\gamma = 2$ in 2D and $\gamma = \frac{5}{3}$ in 3D. At at t = 0

$$\rho_0(r) = \left(\frac{r_e^2 - r^2}{r_e^2 - r_i^2}\rho_i^{\gamma-1} + \frac{r^2 - r_i^2}{r_e^2 - r_i^2}\rho_e^{\gamma-1}\right)^{\frac{1}{\gamma-1}},$$

Numerical results

with $\rho_i = 1$ and $\rho_e = 2$. The initial the pressure is $p_0(r) = \rho_0(r)^{\gamma}$. The initial entropy is uniform $s_0 = \frac{p_0}{\rho_0^2} = 1$. The velocity is $\mathbf{u}_0 = 0$ at t = 0.

Let us denote the sound speed as c. The solution is an isentropic compression ($s = \frac{p}{q\gamma} = 1$) such that the position at time t > 0 is R(r, t) = h(t)r, where the compression rate is $h(t) = \sqrt{1 - \frac{t^2}{\tau_{t-r}^2}}$ and the

focalisation time is

$$\tau_{\rm foc} = \sqrt{\frac{(\gamma-1)(r_e^2-r_i^2)}{2(c_i^2-c_e^2)}}$$



Numerical methods for FCI Part II: Hydrodynamics



Order of convergence

The analytical solution is the continuous line, the discrete solution is plotted with symbols.

Introduction

PDEs

Schemes-

construction

Numerical results

Numerical analysis In 2D we used four meshes : M_1 is a 10 × 10 = 100 cells mesh, that is 10 sectors and and 10 layers; M_2 is 20 × 20 = 400 cells; M_3 is 40 × 40 = 1600 cells; and finally M_4 is 80 × 80 = 6400 cells.

In 3D we use three meshes : the first mesh N_1 has 10 sectors per facets and 5 layers, since the exterior and interior boundary are designed with 3 square meshes, then the total number of cells is

 $3 \times 5 \times 10 \times 10 = 1500$ cells; then we double the number of cells in each direction, that N_2 is a 12000 cells mesh; and finally N_3 is a 96000 cells mesh. The order is one (O_1) or two (O_2) .

d.	m.	0.	$r_i(t_f)$	$r_e(t_f)$	0.	$r_i(t_f)$	$r_e(t_f)$
2	<i>M</i> ₁	<i>O</i> ₁	0.4223	0.4820	<i>O</i> ₂	0.4343	0.4880
2	M ₂	<i>O</i> ₁	0.4392	0.4937	<i>O</i> ₂	0.4458	0.4966
2	M ₃	<i>O</i> ₁	0.4453	0.4975	<i>O</i> ₂	0.4487	0.4991
2	M4	<i>O</i> ₁	0.4478	0.4989	<i>O</i> ₂	0.4495	0.4997
conv. o.			pprox 1.09	≈ 1.18		≈ 1.37	≈ 1.58
3	N1	01	0.4133	0.4833	02	0.4269	0.4885
3	N ₂	<i>O</i> ₁	0.4339	0.4929	<i>O</i> ₂	0.4422	0.4963
3	N ₃	<i>O</i> ₁	0.4424	0.4967	<i>O</i> ₂	0.4472	0.4987
conv. o.			pprox 1.08	≈ 1.10		≈ 1.47	≈ 1.50

Numerical methods for FCI Part II: Hydrodynamics

Numerical analysis

< □ > < □ > < □ > < □ > < □ > .



Introduction

PDEs

Schemesconstruction

Numerical results

Numerical analysis We distinguish 4 properties

Conservation : mass, momentun, total energy

Stability : entropy

under ad-hoc CFL

 $S_j^{k+1} \ge S_j^k \quad \forall j$

$$\max_{j}\left(rac{c_{j}^{k}}{\Delta x_{j}^{k}}
ight)\Delta t^{k}\leq1$$

and

$$\frac{\left|V_j^{k+1}-V_j^k\right|}{V_j^k} \le \frac{1}{10}.$$

Stability : mesh.
 Can we garantee that V_j^k > 0 for all cells j and all time step k ?
 This is completely open.

Convergence to the Euler equations in the Lax sense.



Conservation

The nodal solver writes

Introduction

$$\sum_{j} \mathbf{C}_{jr} \rho_{jr} = 0,$$

$$p_{jr} - p_{j} + \rho_{j} c_{j} \left(\mathbf{u}_{r} - \mathbf{u}_{j}, \mathbf{n}_{jr} \right) = 0, \qquad \mathbf{n}_{jr} = \frac{\mathbf{C}_{jr}}{|\mathbf{C}_{jr}|},$$

PDEs

Schemesconstruction

Numerical results

Numerical analysis The momentum equation $M_i \frac{\mathbf{u}_j^{new} - \mathbf{u}_j}{m_i} = -$

$$A_j \frac{\mathbf{u}_j^{\text{max}} - \mathbf{u}_j}{\Delta t} = -\sum_r \mathbf{C}_{jr} p_{jr}$$

Therefore

$$\sum_{j} M_{j} \frac{\mathbf{u}_{j}^{new} - \mathbf{u}_{j}}{\Delta t} = -\sum_{j} \sum_{r} \mathbf{C}_{jr} \mathbf{p}_{jr} = -\sum_{r} \sum_{j} \mathbf{C}_{jr} \mathbf{p}_{jr} = 0.$$

That is by induction

$$\sum_{j} M_{j} \mathbf{u}_{j}^{new} = \sum_{j} M_{j} \mathbf{u}_{j} = \sum_{j} M_{j} \mathbf{u}_{j}^{ini}.$$

Similarily

$$\sum_{j} M_{j} \frac{e_{j}^{new} - \mathbf{e}_{j}}{\Delta t} = -\sum_{j} \sum_{r} \left(\mathbf{C}_{jr} \cdot \mathbf{u}_{r} \right) p_{jr} = -\sum_{r} \left(\sum_{j} \mathbf{C}_{jr} p_{jr} \cdot \mathbf{u}_{r} \right) = 0.$$

Conservation is insuder at corners, and not at faces as in standard Finite Volume methods.

1



What is the method?

the corner flux equation

and the close contour relation

Answer Use the semi-discrete scheme

Introduction

PDEs

Schemes-

construction

Numerical results

Numerical analysis $\left\{ \begin{array}{ll} M_j \tau_j'(\mathbf{t}) = + \sum_r \left(\mathbf{C}_{jr} \cdot \mathbf{u}_r \right) & \Longleftrightarrow \mathbf{x}_r'(\mathbf{t}) = \mathbf{u}_r, \\ M_j \mathbf{u}_j'(\mathbf{t}) = - \sum_r \mathbf{C}_{jr} P_{jr}, \\ M_j e_j'(\mathbf{t}) = - \sum_r \left(\mathbf{C}_{jr} \cdot \mathbf{u}_r \right) p_{jr} \end{array} \right.$

 $p_{jr} - p_j + \rho_j c_j \left(\mathbf{u}_r - \mathbf{u}_j, \frac{\mathbf{C}_{jr}}{|\mathbf{C}_{jr}|} \right),$

 $\sum {\bf C}_{jr}=0.$

The algebra is

$$T_{j}M_{j}\frac{d}{dt}S_{j} = M_{j}e_{j}'(t) - (\mathbf{u}_{j}, M_{j}\mathbf{u}_{j}'(t)) + \rho_{j}M_{j}\tau_{j}'(t)$$

$$= -\sum_{r} (\mathbf{C}_{jr}, \mathbf{u}_{r}) \rho_{jr} + (\mathbf{u}_{j}, \sum_{r} (\mathbf{C}_{jr}, \mathbf{u}_{r}) \rho_{jr}) + \rho_{j}\sum_{r} (\mathbf{C}_{jr}, \mathbf{u}_{r})$$

$$= \sum_{r} (\mathbf{C}_{jr}, \mathbf{u}_{r} - \mathbf{u}_{j}) (\rho_{jr} - \rho_{j}) \ge 0.$$

CQFD

Entropy



Numerical

Numerical

analysis

Mesh stability in 2D (and nD)



Solution 1 Use only simplices (triangles, tets in 3D) : Theorem (with C. Mazeran). The semi-discrete scheme with simplicies is mesh-stable.

Solution 2 Use a cell-centered scheme with less (no?) spurious modes : the CHIC scheme.

Solution 3 Use ALE (Arbitrary Lagrange Euler). This is easy with cell-centered schemes.

This is still a an open problem. More research is needed.

Э

Convergence à la Lax

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □



oduction	Consider a given numerical scheme for the discretization of the compressible gas dynamics system. Assume that the numerical solution is bounded in L^{∞} and converges in L^1_{loc} to some limit. Assume that we can prove that the limit is a weak solution to						
Es	$\int_{\mathbf{r} \in \mathbb{R}} \int_{-\pi d} \left(\rho \partial_t \varphi + \rho \mathbf{u} \cdot \nabla \varphi \right) dt dx = 0,$	$\forall \varphi \in \mathcal{D}_0,$					
emes- struction	$\begin{cases} \int_{t\in\mathbb{R}} \int_{x\in\mathbb{R}^d} (\rho \mathbf{u} \cdot \partial_t \varphi + \rho \mathbf{u} \otimes \mathbf{u} + \mathbf{pl} \cdot \nabla \varphi) dt dx = 0, \\ \int_{t\in\mathbb{R}} \int_{x\in\mathbb{R}^d} (\rho \mathbf{u} \cdot \partial_t \varphi + \rho \mathbf{u} \otimes \mathbf{u} + \mathbf{pl} \cdot \nabla \varphi) dt dx = 0, \end{cases}$	$\forall \varphi \in \mathcal{D}_0^d,$	(1)				

Numerical

Numerical analysis

 $\begin{array}{ll} \int_{t \in \mathbb{R}} \int_{\mathbf{x} \subset \mathbb{R}^d} (\rho e \partial_t \varphi + \rho \mathbf{e} \mathbf{u} \cdot \nabla \varphi) \, dt dx = 0, & \forall \varphi \in \mathcal{D}_0, \\ \int_{t \in \mathbb{R}} \int_{\mathbf{x} \subset \mathbb{R}^d} (\rho S \partial_t \varphi + \rho S \mathbf{u} \cdot \nabla \varphi) \, dt dx \leq 0, & \forall \varphi \in \mathcal{D}_0^+, \end{array}$

where \mathcal{D}_0 is the set of smooth test functions with compact support, and $\mathcal{D}_0 \subset \mathcal{D}_0$ is the set of smooth non negative test functions with compact support.

We will say that the scheme is weakly consistent.

In that game, we are allowed to add as many stability hypothesis as needed.

Theorem (2010): Cell-centered Lagrangian schees are weakly consistent with the Euler equations of compressible gas dynamics.



Idea of the proof in 1D

Interpolate the mesh :
$$x_{j+\frac{1}{2}}(t) = x_{j+\frac{1}{2}}^{n} + (t-t^{n})u_{j+\frac{1}{2}}^{n}$$
 for $t^{n} \le t \le t^{n+1}$; $\Delta x_{j}(t) = x_{j+\frac{1}{2}}(t) - x_{j-\frac{1}{2}}(t)$.

PDEs

Schemes-

Numerical

Numerical analysis



The red domain is
$$\Theta_j^{n+\frac{1}{2}} = \left\{ t^n < t < t^{n+1}, \quad x_{j-\frac{1}{2}}(t) < x < x_{j+\frac{1}{2}}(t) \right\}.$$

e numerical solution

$$\text{for } (\mathbf{x}, t) \in \Theta_j^{n+\frac{1}{2}}, \text{ set } \begin{cases} \rho(\mathbf{x}, t) = \frac{M_j}{\Delta x_j(t)}, \\ u(\mathbf{x}, t) = u_j^n + \frac{t - t^n}{\Delta t} (u_j^{n+1} - u_j^n), \\ e(\mathbf{x}, t) = e_j^n + \frac{t - t^n}{\Delta t} (e_j^{n+1} - e_j^n), \\ \\ \overline{u}(\mathbf{x}, t) = \frac{x - x_j - \frac{1}{2}(t)}{\Delta x_j(t)} u_{j-\frac{1}{2}}(t) + \frac{x_{j+\frac{1}{2}}(t) - x}{\Delta x_j(t)} u_{j+\frac{1}{2}}(t) \neq u(\mathbf{x}, t). \end{cases}$$

Property One has the identity

$$\partial_t \rho + \partial_x (\rho \overline{u}) = 0 \text{ in } \mathcal{D}'_{x,t}.$$



Results in multiD

One has the formula in the weak sense

$$\partial_t \rho_h + \nabla \cdot (\rho_h \overline{\mathbf{u}}_h) = A^1, \qquad \text{with } A^1 = \sum_j \left[\rho_j \left(\nabla \cdot \overline{\mathbf{u}}_j - \frac{1}{V_j(t)} \int_{\Omega_j(t)} \nabla \cdot \overline{\mathbf{u}}_j dx \right) \right] \mathbf{1}_{\mathbf{x} \in \Omega_j(t)}.$$

One has the formula

$$\partial_t \left(\rho_h \mathbf{u}_h \right) + \nabla \cdot \left(\rho_h \mathbf{u}_h \otimes \overline{\mathbf{u}}_h \right) = B^1 + B^2 + B^3$$

in the weak sense, where the interpolation error in space is

$$B^{1} = \sum_{j} \left[\rho_{j} \mathbf{u}_{j} \left(\nabla . \overline{\mathbf{u}}_{j} - \frac{1}{V_{j}(t)} \int_{\Omega_{j}(t)} \nabla . \overline{\mathbf{u}}_{j} dx \right) \right] \mathbf{1}_{\mathbf{x} \in \Omega_{j}(t)},$$

the interpolation error in time is

$$B^{2} = -\sum_{j} \left[\left(\frac{\mathbf{1}_{\mathbf{x} \in \Omega_{j}(t)}}{V_{j}(t)} - \frac{\mathbf{1}_{\mathbf{x} \in \Omega_{j}^{k}}}{V_{j}^{k}} \right) \sum_{j} \mathbf{C}_{jr}^{k} p_{jr}^{k} \right],$$

and the approximation of $-\nabla p$ is

$$B^{3} = -\sum_{j} \left[\sum_{r} \mathbf{C}_{jr}^{k} p_{jr}^{k} \right] \frac{\mathbf{1}_{\mathbf{x} \in \Omega_{j}^{k}}}{V_{j}^{k}}.$$

1

Schemesconstruction

PDEs

Numerical results

Numerical analysis

Fundamental property

イロト イヨト イヨト イヨト



Theorem

PDEs

Schemesconstruction

Numerical results

Numerical

analysis

Assume that the speed of sound is within the bounds
$$0 < \alpha_1 \le \rho_j c_j < \alpha_2$$
 everywhere. Assume that the mesh is regular in the sense $\alpha_3 h^d \le V_j$ and diam $(\Omega_j) \le \alpha_4 h$ for all cells, with uniform constants $\alpha_3, \alpha_4 > 0$. Assume that (p_j) and (\mathbf{u}_j) are bounded in L^{∞} and are bounded in BV in the sense

$$\sum_{j} \sum_{k \in V(j)} h^{d-1} \left| p_j - p_k \right| \leq \alpha_5 \text{ and } \sum_{j} \sum_{k \in V(j)} h^{d-1} \left| \mathbf{u}_j - \mathbf{u}_k \right| \leq \alpha_6.$$

Then B=abla p+O(h) in the weak sense. The residual O(h) depends on the smooth test function $arphi\in \mathcal{C}_0^2$.

The key property is the identity

$$\sum_{r} \mathbf{C}_{jr} \otimes \mathbf{x}_{r} = V_{j} \mathbf{I}_{d}$$

where $\mathbf{I}_d \in \mathbf{R}^{d \times d}$ stands for the identity matrix in dimension d.

The same identity seems essential in the recent works Droniou, Eymard, Herbin,Gallouet about the consistency of the diffusion equation.

Э



Conclusion of the day

イロト イポト イヨト イヨト

						-		
	0		Le 1	-	L	9		

PDEs

- Schemes-
- construction
- Numerical results
- Numerical analysis

- Lagrangian methods are central for the simulation of ICF flows.
- Ongoing research show good potential of cell-centered schemes. The CHIC scheme is now routinely used for Direct Drive at CELIA.
- GLACE is less viscous (more accurate) than CHIC, but needs more stabilization.
- In 3D, GLACE is more natural than CHIC.
- Weak consistency is proved. It validates the use of such methods for ICF compressible flows with shocks.
- Coupling with radiation is an issue.

Э