

# Vortex dynamics and Compressibility effects in Large-Eddy Simulations (1 of 2)

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## Outline:

- Talk 1
  - ▷ Mixing layers (*al.*, J. Silvestrini *et al.*, *Eur. J. Mech. B*, **17**, 1998)
  - ▷ LES in Fourier space
  - ▷ LES in physical space
  - ▷ SGS model assessment
  - ▷ Compressible LES formulations
  - ▷ Air-intake flow (unpublished)

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## Outline (cont'd):

- Talk 2
  - ▷ spatial discretization
  - ▷ High-order conservation schemes
  - ▷ MILES ENO assessment
  - ▷ example of shock-wave/boundary layer interaction
  - ▷ Cavity flows (Y. Dubief)
  - ▷ Cavity flows (L. Larchevêque *et al.*, *Phys. Fluids, Phys. Fluids*, **15**, 2003, *J. Fluid Mech.*, **516**, 2004)
  - ▷ Supersonic compression ramp flows (unpublished)
  - ▷ Solid-propellant rocket flow (unpublished)
  - ▷ Separation control by tangential blowing (preliminary)
  - ▷ Supersonic channel flow (C. Brun *et al.*, ETC5, Toulouse, 2003)
  - ▷ MHD mixing layers and jets (H. Baty *et al.*, *Phys. Plasmas*, **10**, 2003)

## Acknowledgements

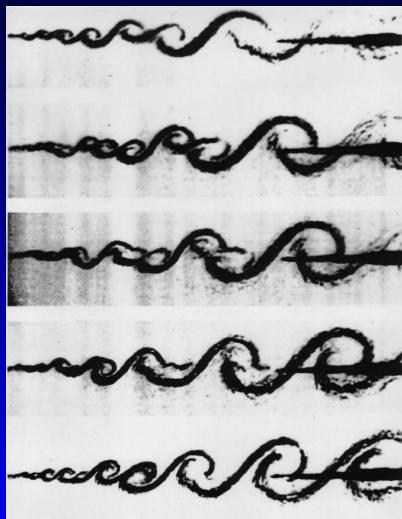
- H. Baty
- E. Briand
- C. Brun
- E. David
- M. Haberkorn
- P. Kessler
- L. Larchevêque
- E. Schwander
- J.H. Silvestrini
- LEGI Grenoble, M. Lesieur, O. Métais
- ONERA Chatillon
- Observatoire de Strasbourg

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## Mixing layers (1/10)

- pairings (Konrad, 1976)



## Mixing layers (2/10)

- three-dimensionality (Breidenthal, 1982)

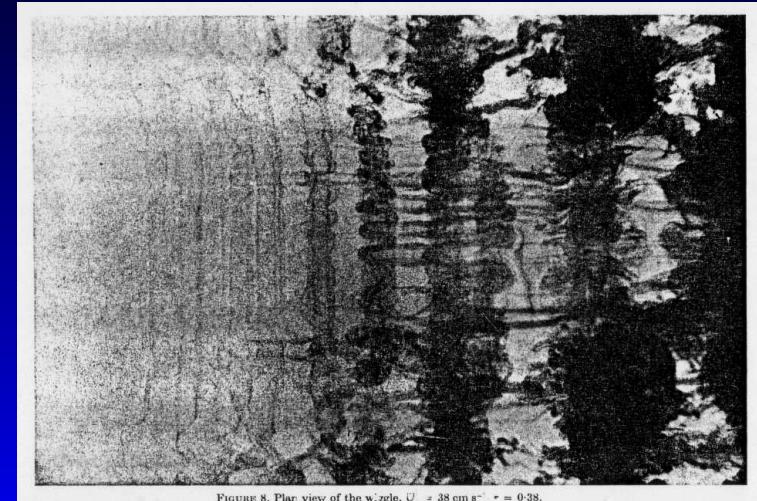
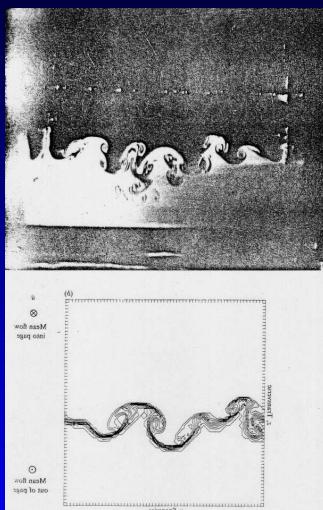


FIGURE 8. Plan view of the w. ggle,  $U_1 = 38 \text{ cm s}^{-1}$ ,  $\tau = 0.38$ .

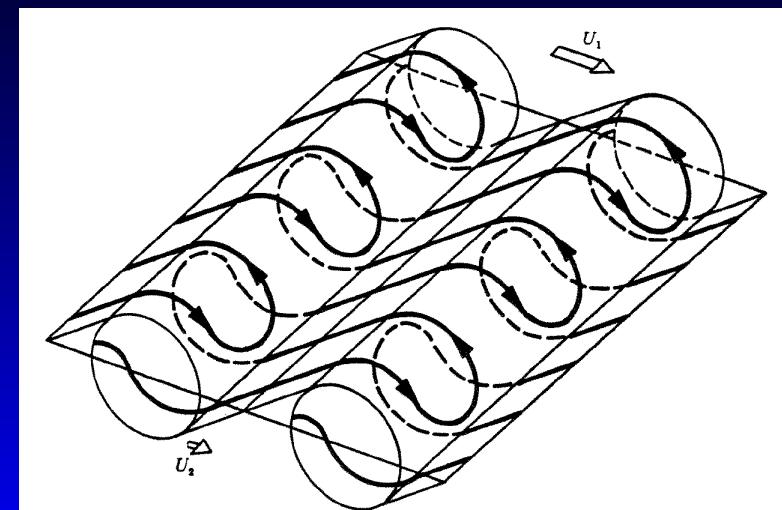
## Mixing layers (3/10)

- "rib"-vortices (Bernal *et al.*, 1986; Metcalfe *et al.*, 1986)



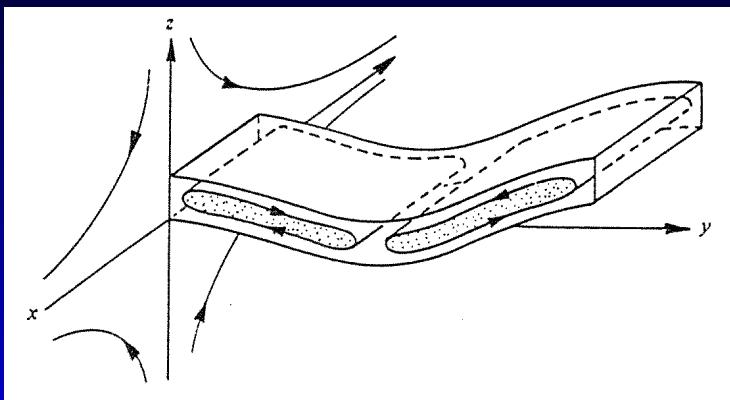
## Mixing layers (4/10)

- conceptual model (Bernal *et al.*, 1986)



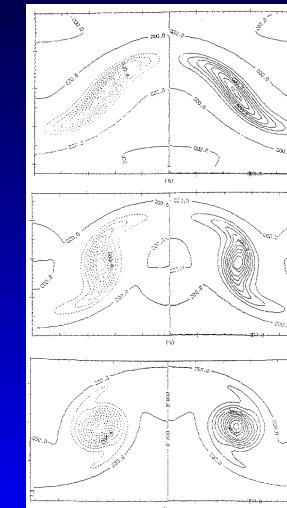
## Mixing layers (5/10)

- Hyperbolic instability (Lin & Corcos, 1982)



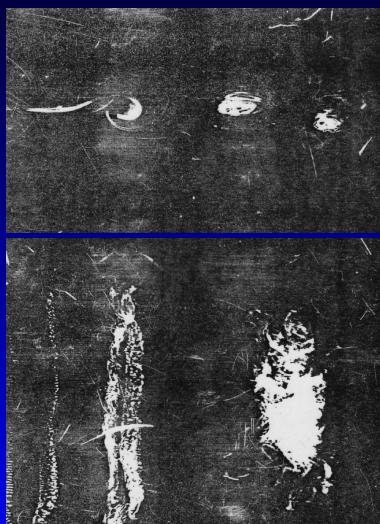
## Mixing layers (6/10)

- Hyperbolic instability (Lin & Corcos, 1982)



## Mixing layers (7/10)

- Helical pairings (Chandrsuda *et al.*, 1978)



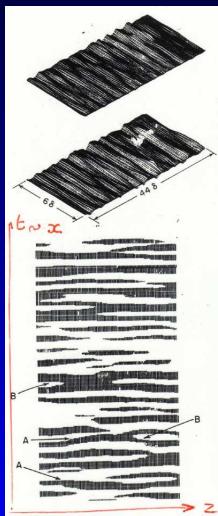
## Mixing layers (8/16)

- Helical pairings (Chandrsuda *et al.*, 1978)



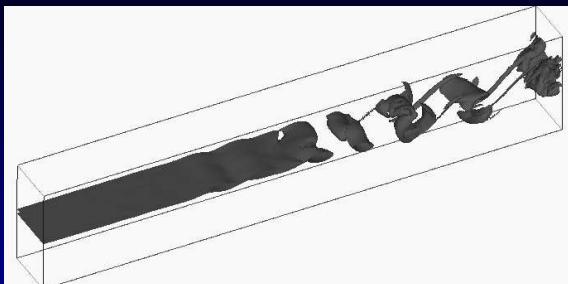
## Mixing layers (9/10)

- Dislocations/Branchings/Defects (Browand, 1982)

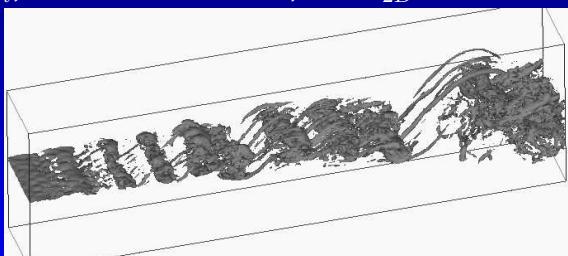


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## Spatial mixing layers (1/5)



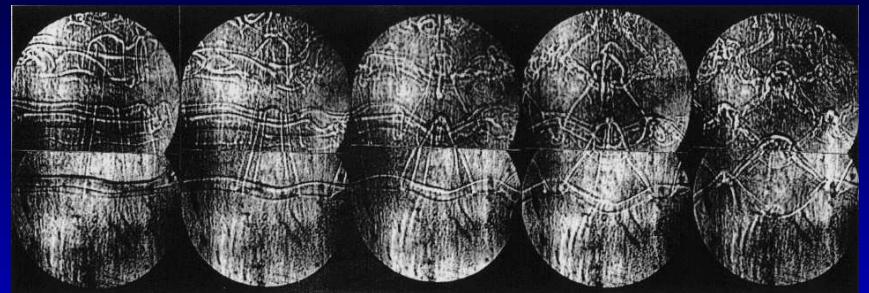
$\|\vec{\omega}\| = 1/3 \omega_i$ , in DNS at  $Re = 100$ , with  $\varepsilon_{2D} = 10^{-4}$  and  $\varepsilon_{1D} = 10^{-3}$ .



$\|\vec{\omega}\| = 2/3 \omega_i$ , in LES at  $\nu = 0$ , with  $\varepsilon_{2D} = 10^{-5}$  and  $\varepsilon_{1D} = 10^{-4}$ .

## Mixing layers (10/10)

- Helical pairings / Chain-fence-like vortices (Nygaard & Glezer, 1992)



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## Spatial mixing layers (2/5)

LES  $(L_x, L_y) = (16\lambda_i, 4\lambda_i)$ ,  $(N_x, N_y) = (384, 96)$

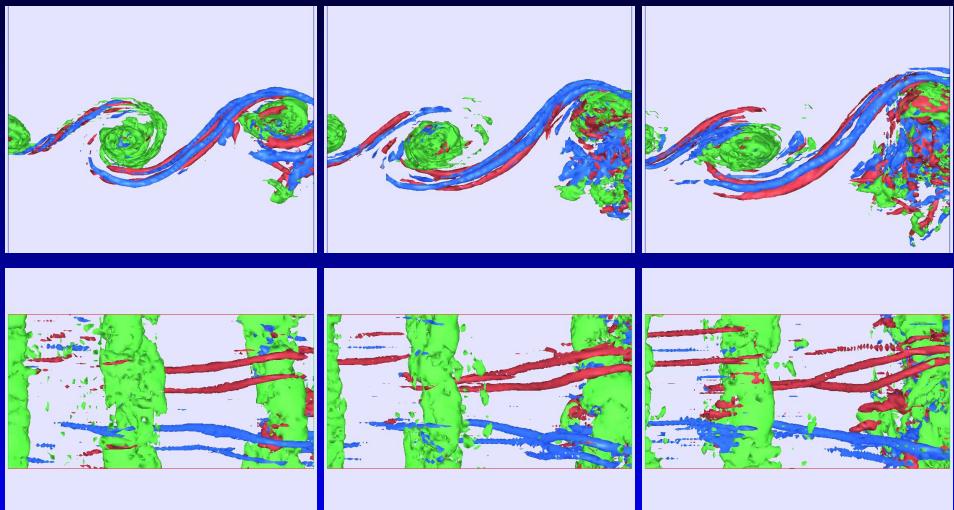
- narrow domain:  $L_z = 2 \lambda_i$ ,  $N_z = 48$ 
  - ▷ side view
  - ▷ pressure
  - ▷ vorticity
- wider domain:  $L_z = 4 \lambda_i$ ,  $N_z = 96$ 
  - ▷ pressure
  - ▷ vorticity



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## Spatial mixing layers (3/5)

- Multiple-stage roll-up & pairing



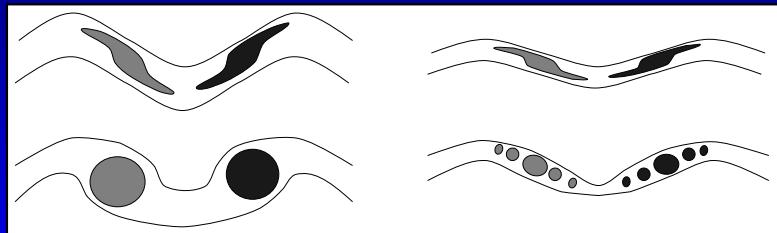
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## Spatial mixing layers (4/5)

- DNS,  $Re = 100$
- $(L_x, L_y) = (16\lambda_i, 4\lambda_i)$ ,  $(N_x, N_y) = (480, 96)$
- narrow domain:  $L_z = 2 \lambda_i$ ,  $N_z = 48$
- forcing amplitude:  $0.05U$
- $\|\vec{\omega}\| = 3/4 \omega_i$

## Spatial mixing layers (4/5)

- as conjectured by Lin & Corcos, *J. Fluid Mech.*, **141**, 139–178 (1978).  
*... In a layer where the sign of the vorticity alternates (in the direction along which strain is absent), each portion of the layer that contains vorticity of a given sign eventually contributes that vorticity to a single vortex. This may occur in a single stage if the initial layer thickness is not excessively small next to the spanwise extent of vorticity of a given sign or, otherwise, in a succession of stages involving local roll-up and pairing.*



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## LES in Fourier space (1/8)

- Navier-Stokes in Fourier space (statistical homogeneity)

$$\hat{u}_i(\underline{k}, t) = \left( \frac{1}{2\pi} \right)^3 \int e^{-i\underline{k} \cdot \underline{x}} u_i(\underline{x}, t) d\underline{x}$$

$$\begin{aligned} \frac{\partial}{\partial t} \hat{u}_i(\underline{k}, t) + \nu k^2 \hat{u}_i(\underline{k}, t) = \\ - ik_m \left( \delta_{ij} - \frac{k_i k_j}{k^2} \right) \int_{\underline{p}+\underline{q}=\underline{k}} \hat{u}_j(\underline{p}, t) \hat{u}_m(\underline{q}, t) d\underline{p} \end{aligned}$$



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## LES in Fourier space (2/8)

- Passive scalar

$$\hat{T}(\underline{k}, t) = \left( \frac{1}{2\pi} \right)^3 \int e^{-i\underline{k} \cdot \underline{x}} T(\underline{x}, t) d\underline{x}$$

$$\begin{aligned} \frac{\partial}{\partial t} \hat{T}(\underline{k}, t) + \kappa k^2 \hat{T}(\underline{k}, t) = \\ - ik_j \int_{\underline{p}+\underline{q}=\underline{k}} \hat{u}_j(\underline{p}, t) \hat{T}(\underline{q}, t) d\underline{p} \end{aligned}$$



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## LES in Fourier space (3/8)

- Low-pass filter (sharp filter):

$$\bar{\hat{f}} = \hat{f} \text{ for } |\underline{k}| < k_C = \pi/\Delta x, \bar{\hat{f}} = 0 \text{ for } |\underline{k}| > k_C$$

- Spectral eddy viscosity (Heisenberg, Kraichnan . . .):

$$\begin{aligned} \frac{\partial}{\partial t} \hat{u}_i(\underline{k}, t) + [\nu + \nu_t(k|k_C)] k^2 \hat{u}_i(\underline{k}, t) = \\ - ik_m \left( \delta_{ij} - \frac{k_i k_j}{k^2} \right) \int_{\underline{p}+\underline{q}=\underline{k}}^{|\underline{p}|, |\underline{q}| < k_C} \hat{u}_j(\underline{p}, t) \hat{u}_m(\underline{q}, t) d\underline{p} \end{aligned}$$

with



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## LES in Fourier space (4/8)

- Spectral eddy viscosity  $\nu_t(k|k_C)$ :

$$\begin{aligned} \nu_t(k|k_C) k^2 \hat{u}_i(\underline{k}, t) = \\ ik_m \left( \delta_{ij} - \frac{k_i k_j}{k^2} \right) \int_{\underline{p}+\underline{q}=\underline{k}}^{|\underline{p}| \text{ or } |\underline{q}| > k_C} \hat{u}_j(\underline{p}, t) \hat{u}_m(\underline{q}, t) d\underline{p} \end{aligned}$$

- Spectral eddy diffusivity  $\kappa_t(k|k_C)$ :

$$\begin{aligned} \kappa_t(k|k_C) k^2 \hat{T}(\underline{k}, t) = \\ ik_j \int_{\underline{p}+\underline{q}=\underline{k}}^{|\underline{p}| \text{ or } |\underline{q}| > k_C} \hat{u}_j(\underline{p}, t) \hat{T}(\underline{q}, t) d\underline{p} \end{aligned}$$



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## LES in Fourier space (5/8)

- Spectral eddy diffusivity  $\kappa_t(k|k_C)$  satisfies:

$$\begin{aligned} \frac{\partial}{\partial t} \hat{T}(\underline{k}, t) + [\kappa + \kappa_t(k|k_C)] k^2 \hat{T}(\underline{k}, t) = \\ - ik_j \int_{\underline{p}+\underline{q}=\underline{k}}^{|\underline{p}|, |\underline{q}| < k_C} \hat{u}_j(\underline{p}, t) \hat{T}(\underline{q}, t) d\underline{p} \end{aligned}$$

- Two-point stochastic closures (EDQNM, TFM, LHDIA . . .) provide model expressions for  $\nu_t(k|k_C)$  and  $\kappa_t(k|k_C)$



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## LES in Fourier space (6/8)

- Spectral-peak eddy coefficients: EDQNM —→

$$\nu_t(k|k_C) = \left[ \frac{E(k_C)}{k_C} \right]^{1/2} \nu_t^+ \left( \frac{k}{k_C} \right)$$

assuming  $E(k) \sim k^{-5/3}$  for  $k \gtrsim k_C$

- Asymptotics:  $\nu_t^+ \left( \frac{k}{k_C} \right) \rightarrow 0.441 C_K^{-3/2} \sim 0.28$  when  $\frac{k}{k_C} \rightarrow 0$
- reminder: (isotropic) energy spectrum  $E(k)$ :

$$E(k, t) = 2\pi k^2 \langle \hat{u}(\underline{k}, t) \cdot \hat{u}^*(\underline{k}, t) \rangle_{\|\underline{k}\|=k}$$

$$\frac{1}{2} \langle \underline{u} \cdot \underline{u} \rangle = \int E(k) dk$$



## LES in Fourier space (8/8)

- Spectral-dynamic model (Lesieur-Métais-Lamballais, 1996): for  $E(k) \sim k^{-m}$  at  $k_C$ . The value of the plateau is recomputed using EDQNM non-local expansions, the peak is unchanged —→

$$\nu_t(k|k_C) = 0.31 \frac{5-m}{m+1} \sqrt{3-m} C_K^{-3/2} \left[ \frac{E(k_C)}{k_C} \right]^{1/2} \nu_t^+ \left( \frac{k}{k_C} \right)$$

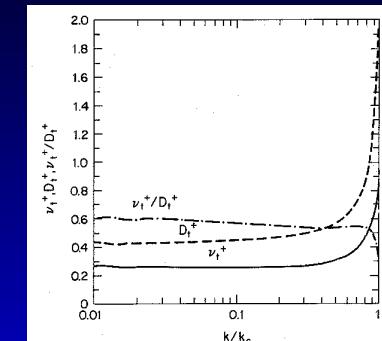
$$Pr_t = 0.18 (5-m)$$

whenever  $m \leq 3$ , otherwise  $\nu_t = 0$ .



## LES in Fourier space (7/8)

- EDQNM non-dimensional eddy coefficients:  $\nu_t^+$ ,  $\kappa_t^+ = \frac{\nu_t^+}{Pr_t}$



- —→  $Pr_t \approx 0.6$

## LES in physical space (1/10)

- Physical space (*finite-differences methods, or finite-volume...*),  $\rho$  uniform, grid of mesh  $\Delta x$
- low-pass spatial filter  $G_{\Delta x}$ , cut-off scale  $\Delta x$

$$\bar{f}(x, t) = f * G_{\Delta x} = \int f(\underline{y}, t) G_{\Delta x}(x - \underline{y}) d\underline{y}.$$

- filter commutes with space and time derivatives (if mesh uniform).



## LES in physical space (2/10)

- Navier-Stokes equations

$$\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_j}(u_i u_j) = -\frac{1}{\rho_0} \frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j}(2\nu S_{ij})$$

with  $S_{ij} = (1/2)(\partial u_i / \partial x_j + \partial u_j / \partial x_i)$ , strain-rate tensor

- filtered equations :

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j}(\bar{u}_i \bar{u}_j) = -\frac{1}{\rho_0} \frac{\partial \bar{p}}{\partial x_i} + \frac{\partial}{\partial x_j}(2\nu \bar{S}_{ij} + T_{ij})$$

with  $T_{ij} = \bar{u}_i \bar{u}_j - \bar{u}_i \bar{u}_j$  , SubGrid-Stress tensor



## LES in physical space (4/10)

- Smagorinsky model

▷ *a la* Prandtl mixing length argument:  $\nu_t \sim \Delta x v_{\Delta x}$

▷  $v_{\Delta x} \sim \frac{\partial v}{\partial x} \Delta x$

▷  $v_{\Delta x} = \Delta x |\bar{S}|$ , with  $|\bar{S}| = \sqrt{2\bar{S}_{ij}\bar{S}_{ij}}$ .

▷ →

$$\nu_t = (C_S \Delta x)^2 |\bar{S}|$$

▷ inertial arguments →  $C_S \approx \frac{1}{\pi} \left( \frac{3C_K}{2} \right)^{-3/4} \rightarrow C_S \approx 0.18$  for  $C_K = 1.4$

## LES in physical space (3/10)

- eddy-viscosity assumption (Boussinesq):

$$T_{ij} = 2\nu_t(\underline{x}, t) \bar{S}_{ij} + \frac{1}{3} T_{ll} \delta_{ij}$$

- LES momentum equations

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j}(\bar{u}_i \bar{u}_j) = -\frac{1}{\rho_0} \frac{\partial \bar{P}}{\partial x_i} + \frac{\partial}{\partial x_j}[2(\nu + \nu_t) \bar{S}_{ij}]$$

- continuity:  $\partial \bar{u}_j / \partial x_j = 0$ ,
- macro pressure  $\bar{P} = \bar{p} - (1/3)\rho_0 T_{ll}$ .
- models: Smagorinsky, structure-function, dynamic Smagorinsky ...



## LES in physical space (5/10)

- Structure-function model (Métais-Lesieur, *J. Fluid Mech.*, 1992)

$$\nu_t^{SF}(\underline{x}, \Delta x, t) = 0.105 C_K^{-3/2} \Delta x [\bar{F}_2(\underline{x}, \Delta x, t)]^{1/2}$$

with the 2nd-order velocity structure-function at scale  $\Delta x$

$$\bar{F}_2(\underline{x}, \Delta x, t) = \langle \|\bar{u}(\underline{x}, t) - \bar{u}(\underline{x} + \underline{r}, t)\|^2 \rangle_{\|\underline{r}\|=\Delta x}$$

▷ consistent with the spectral peak model thru (Batchelor)

$$\langle \bar{F}_2(\underline{x}, \Delta x, t) \rangle_{\underline{x}} = 4 \int_0^{k_c} E(k, t) \left( 1 - \frac{\sin(k\Delta x)}{k\Delta x} \right) dk .$$

▷ In the limit of  $\Delta x \rightarrow 0$

$$\nu_t^{SF} \approx 0.777 (C_S \Delta x)^2 \sqrt{2\bar{S}_{ij}\bar{S}_{ij} + \bar{\omega}_i \bar{\omega}_i}$$



## LES in physical space (6/10)

- Filtered Structure Function model (Ducros *et al.*, *J. Fluid Mech.*, 326, 1-36, 1996)

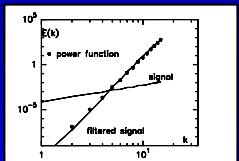
$$\nu_t^{FSF} = 0.0014 C_K^{-\frac{3}{2}} \Delta x \left[ \check{F}_{2_{\Delta x}}(\underline{x}, \Delta x) \right]^{\frac{1}{2}}$$

▷ density-weighted filtered variables:  $\tilde{u} = \frac{\rho \underline{u}}{\rho}$

$$\check{F}_{2_{\Delta x}}(\underline{x}, t) = \langle \|\check{u}(\underline{x} + \underline{r}, t) - \check{u}(\underline{x}, t)\|^2 \rangle_{\|\underline{r}\|=\Delta x}$$

▷  $\check{u}$ : convolution of  $\tilde{u}$  by 2nd-order centered finite-difference Laplacian filter, iterated 3 times

$$\tilde{E}(k) \approx 40^3 \left( \frac{k}{k_C} \right)^9$$



▷  $\sim$  hyperviscosity ; spectral-peak ; ADM

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## LES in physical space (8/10)

- Mixed Scale model (Sagaut, Ta Phuoc)

$$\nu_t^{MS} = C_m(\alpha) |\tilde{S}|^\alpha (q_c^2)^{\frac{(1-\alpha)}{2}} \Delta^{(1+\alpha)} \quad (1)$$

$$q_c^2 = \frac{1}{2} (\tilde{u}_k - \hat{\tilde{u}}_k)^2 \quad (2)$$

▷ Gaussian test filter

$$\hat{\tilde{u}}_i = \frac{1}{4} [\tilde{u}_{i-1} + 2\tilde{u}_i + \tilde{u}_{i+1}] \quad (3)$$

▷  $\alpha = 1 \rightarrow$  Smagorinsky's model

▷  $\alpha = 0 \rightarrow$  Bardina's TKE model

▷ inertial arguments yield  $C_m(\alpha) = 0.06$  for  $\alpha = 1/2$ .

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## LES in physical space (7/10)

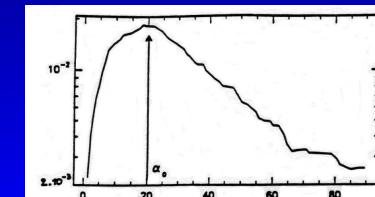
- Selective Structure-Function model David, 1992

$$\nu_t^{SSF} = 0.16 \Phi_{20^\circ}(\underline{x}, t) C_K^{-\frac{3}{2}} \Delta x \left[ \overline{F}_{2_{\Delta x}}(\underline{x}, \Delta x) \right]^{\frac{1}{2}}$$

$$\Phi_{\alpha_0}(\underline{x}, t) = \begin{cases} 1 & \text{if } (\omega, \check{\omega}) \geq 20^\circ \\ 0 & \text{otherwise} \end{cases} .$$

with

$$\check{\omega}(\underline{x}, t) = \langle \omega(\underline{x} + \underline{r}, t) \rangle_{\|\underline{r}\| \leq \Delta x} .$$



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## LES in physical space (9/10)

- Selective Mixed Scale model (Sagaut *et al.*)

$$\nu_t^{SMS} = 0.06 f_{\theta_0} |\tilde{S}|^{1/2} (q_c^2)^{1/4} \Delta^{3/2} , \quad (4)$$

▷ Mixed Scale model with the selection function

$$f_{\theta_0}(\theta) = \begin{cases} 1 & \text{if } \theta \geq \theta_0 \\ r(\theta)^n & \text{otherwise} \end{cases} \quad (5)$$

in which

$$r(\theta) = \frac{\tan^2(\theta/2)}{\tan^2(\theta_0/2)} \quad ; \quad n = 2 \quad (6)$$

instead of David's

$$f_{\theta_0}(\theta) = \begin{cases} 1 & \text{if } \theta \geq \theta_0 \\ 0 & \text{otherwise} \end{cases} \quad (7)$$

still with  $\theta_0 = 20^\circ$ .

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## LES in physical space (10/10)

- Hybrid models (Sagaut et al.)
  - ▷ Scale similarity model

$$\frac{\mathcal{T}_{ij}}{\bar{\rho}} = \tilde{u}_i \tilde{u}_j - \widetilde{u_i u_j} \equiv L^m{}_{ij} = \widehat{\tilde{u}_i \tilde{u}_j} - \widetilde{\tilde{u}_i \tilde{u}_j} \quad (8)$$

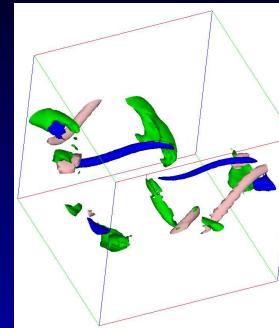
- ▷  $L^m{}_{ij}$ : Resolved Subgrid Stress Tensor
- ▷ a la Bardina if filters  $\sim$  and  $\widehat{\cdot}$  are both defined at grid level  $\Delta$   
(even if the Gaussian filter  $\widehat{\tilde{u}_i} = \frac{1}{4} [\tilde{u}_{i-1} + 2\tilde{u}_i + \tilde{u}_{i+1}]$  is wider than the grid filter  
(box filter))
- ▷ a la Germano, if  $\widehat{\cdot}$  is at scale  $2\Delta$
- Hybridation with an eddy-viscosity model

$$\mathcal{T}_{ij} = \frac{1}{2} \bar{\rho} \left( L^m{}_{ij} + \nu_t \widetilde{S_{ij}} \right) \quad (9)$$

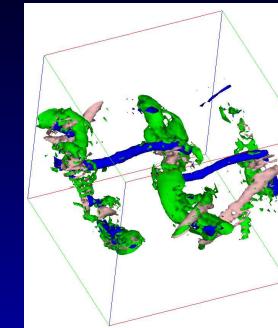
- See Lenormand *et al.*, AIAA, 38, 8, pp. 1340-1350 for assessment in channel flow at Mach 0.5 and 1.5.

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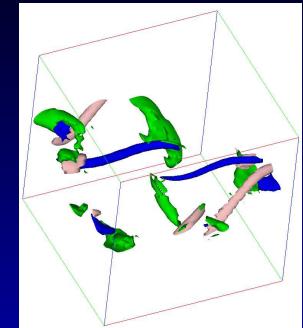
## SGS models assessment:



Smagorinsky model:  
 $\max |\omega_1| = 2.92 \omega_i$



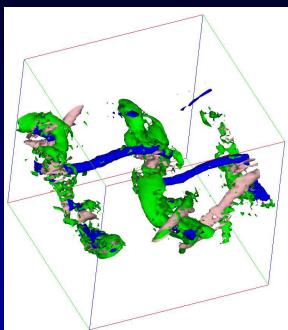
Spectral-Cusp model:  
 $\max |\omega_1| = 4.75 \omega_i$



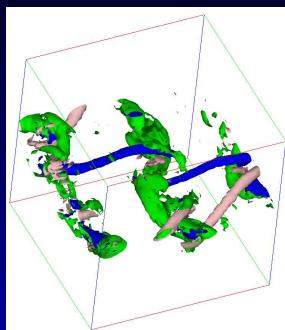
Structure-Function model :  
 $\max |\omega_1| = 2.86 \omega_i$

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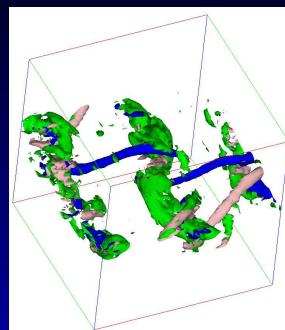
## "smarter" SGS models



Spectral-Cusp model:  
 $\max |\omega_1| = 4.75 \omega_i$



Filtered Structure-Function model :  
 $\max |\omega_1| = 4.83 \omega_i$

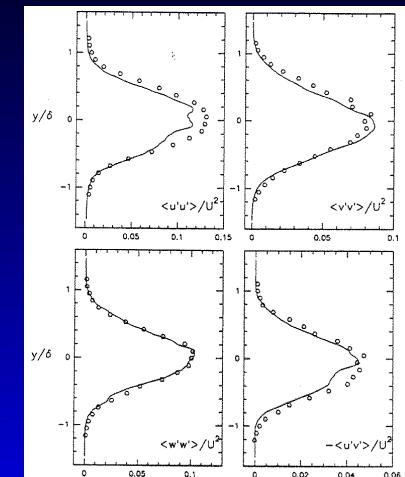


Selective Structure-Function model :  
 $\max |\omega_1| = 5.42 \omega_i$

Further reading: LESIEUR, M. & MÉTAIS, O. (1996) 'New trends in large-eddy simulations of turbulence', *Ann. Rev. Fluid Mech.*, **28**, 45-82.

## SGS models assessment (2/3):

- Reynolds stresses

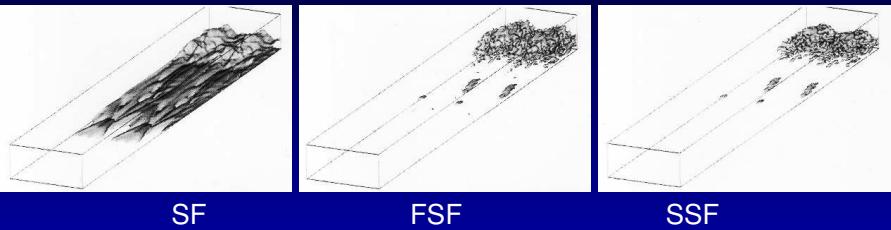


Lines: LES, spectral-dynamic model.  
Symbols: exp. Bell & Mehta (1990)



## SGS models assessment (3/3):

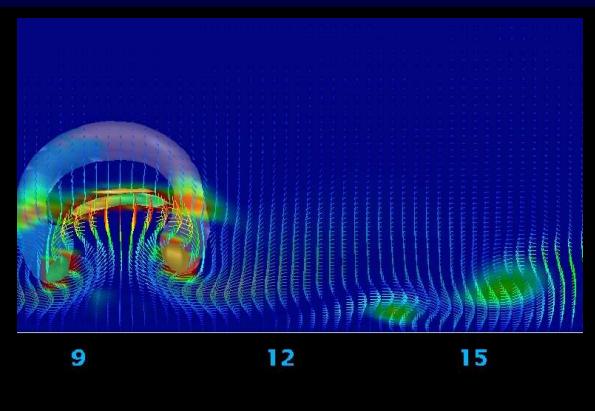
- Transitional boundary layer (simulated with FSF model (Ducros *et al.* *J. Fluid Mech.*, 336, 1996)):  $\nu_t = 2/3 \nu$



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## Boundary layers (2/4)

- H-type transition, grid 1



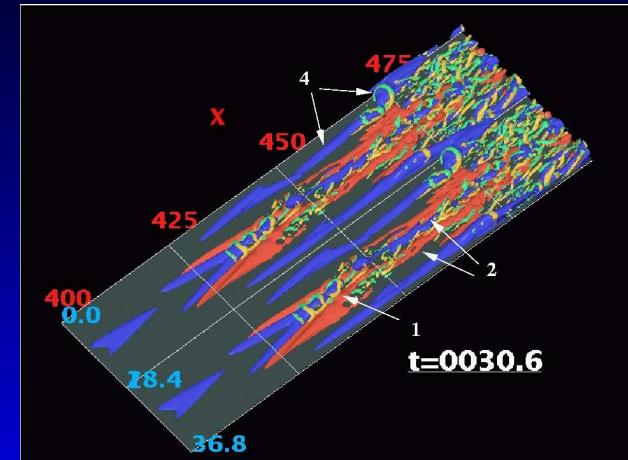
$u' = +0.18 U_\infty$  (red),  $u' = -0.18 U_\infty$  (blue),  
 $Q = 0.1 U_\infty^2 / \delta_1^2$  ( $\omega_x > 0$ ,  $\omega_x < 0$ ).



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## Boundary layers (1/4)

- K-type transition, grid 2

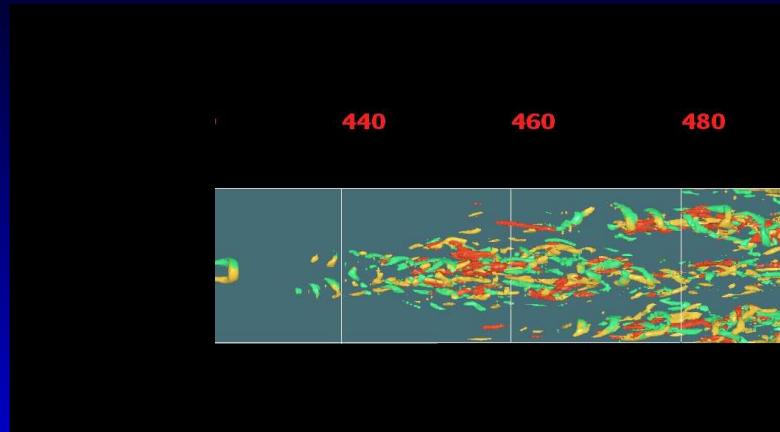


$u' = +0.18 U_\infty$  (red),  $u' = -0.18 U_\infty$  (blue),  
 $Q = \frac{1}{2}(\Omega_{ij}\Omega_{ij} - S_{ij}S_{ij}) = \frac{1}{2\rho}\nabla^2 P = 0.1 U_\infty^2 / \delta_1^2$  ( $\omega_x > 0$ ,  $\omega_x < 0$ )

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## Boundary layers (3/4)

- Is the SGS model intelligent ?

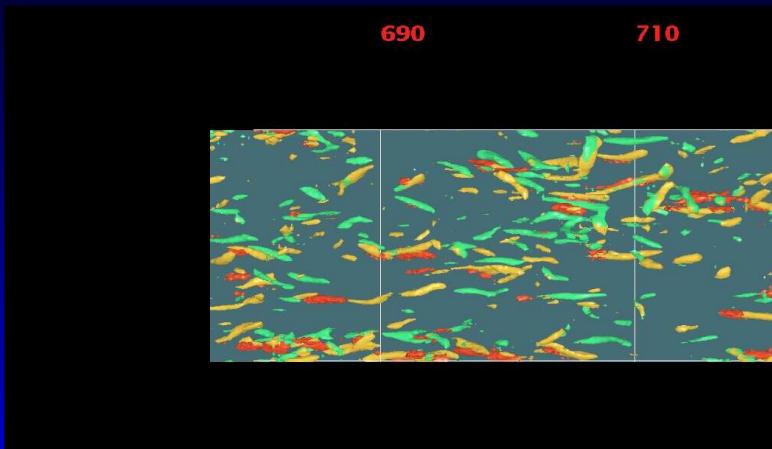


Transitional portion:  
 $\nu_t = 0.5\nu$  (red);  
 $Q = 0.1 U_\infty^2 / \delta_1^2$  ( $\omega_x > 0$ ,  $\omega_x < 0$ ).

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## Boundary layers (4/4)

- Is the SGS model intelligent ?



Turbulent portion:

$$\nu_t = 0.5\nu \text{ (red);}$$

$$Q = 0.1 U_\infty^2 / \delta_1^2 \text{ (\omega}_x > 0, \omega_x < 0\text{).}$$

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## Compressible LES Formulations (2/19)

- Newton and Fourier laws:

$$\underline{\underline{\sigma}} = 2\mu(T)\underline{\underline{S}}_0 + \mu_v \underline{\text{div}} \underline{\underline{u}} , \quad \underline{q} = -k(T) \underline{\text{grad}} T$$

$$\underline{\underline{S}}_0 = \frac{1}{2} \left( \underline{\underline{\underline{\underline{\sigma}}}} \underline{\underline{u}} + {}^t \underline{\underline{\underline{\sigma}}} \underline{\underline{u}} \right) - \frac{1}{3} \underline{\text{div}} \underline{\underline{u}}$$

- Filtered ideal-gas equations of state (13)

$$\bar{p} = R \bar{\rho} \bar{T}, \quad \bar{\rho E} = C_v \bar{\rho T} + \frac{1}{2} \bar{\rho} \underline{\underline{u}} \cdot \underline{\underline{u}} = \bar{p}/(\gamma - 1) + \frac{1}{2} \bar{\rho} \underline{\underline{u}} \cdot \underline{\underline{u}},$$

correct up to about 600K in air, with  $\gamma = C_p/C_v = 1.4$ .

## Compressible LES Formulations (1/19)

- Filtering of direct application of conservation principles:

$$\frac{\partial \bar{\rho}}{\partial t} + \underline{\text{div}} (\bar{\rho} \underline{\underline{u}}) = 0 \quad (10)$$

$$\frac{\partial \bar{\rho} \underline{\underline{u}}}{\partial t} + \underline{\text{div}} (\bar{\rho} \underline{\underline{u}} \otimes \underline{\underline{u}} + \bar{p} \underline{\underline{I}} - \underline{\underline{g}}) = 0 \quad (11)$$

$$\frac{\partial \bar{\rho E}}{\partial t} + \underline{\text{div}} \left[ (\bar{\rho E} + \bar{p}) \underline{\underline{u}} + \underline{\underline{g}} - \underline{\underline{\sigma}} \underline{\underline{u}} \right] = 0 \quad (12)$$

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## Compressible LES Formulations (3/19)

- Beyond 600K,  $\gamma \nearrow$  (vibrations of polyatomic molecules).
- $\mu_v$  never zero in polyatomic molecules, and can be  $\gg \mu$  across shocks (Smits & Dussauge, 1996).
- $\rightarrow$  Stokes hypothesis ( $\underline{\underline{\sigma}}$  trace-free) also excludes shocks.
- in monoatomic gases, helium or argon (no vibration nor rotation),  $\gamma = 5/3$  until ionization and  $\mu_v = 0$ .
- Sutherland's law for  $\mu$  valid between 100K and 1900K. Constant  $Pr = 0.7$  valid in air, even beyond 600K.

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## Compressible LES Formulations (4/19)

- specificity of filtered conservative equations : triple correlation ( $\frac{1}{2}\rho\bar{u}\cdot\bar{u}$ ) involved in a time derivative.
- 2 approaches:
  - ▷ Reynolds filtering
  - ▷ Favre filtering



## Compressible LES Formulations (5/19)

- Non-density-weighted variables (e.g. Boersma & Lele, 1999, CTR Briefs, 365-377).
  - ▷ resolved variables ( $\bar{\rho}, \bar{u}, \bar{p}, \bar{T}$ )
  - ▷ continuity equation (46a) becomes

$$\frac{\partial \bar{\rho}}{\partial t} + \operatorname{div}(\bar{\rho} \bar{u}) = -\operatorname{div}(\bar{p} \bar{u} - \bar{\rho} \bar{u}) \quad (13)$$

- ▷ exact pointwise mass preservation lost, but r.h.s. is conservative and  $\int_{\Omega} r.h.s.$  can be zero, with appropriate flux corrections (in 3D FV or conservative FD).



## Compressible LES Formulations (6/19)

- Non-density-weighted variables (cont'd)
  - ▷ weakly-dissipative model of r.h.s. could increase robustness drastically (as in A.D.M., Leonard, Adams, Stoltz).
  - ▷ closure of  $\frac{1}{2}\rho\bar{u}\cdot\bar{u}$ : secondary issue



## Compressible LES Formulations (7/19)

- Density-weighted variables:  $\tilde{\phi} = \frac{\rho \phi}{\bar{\rho}}$ ,  
 $\forall \phi \notin [\rho, p]$ 
  - ▷ resolved variables ( $\bar{\rho}, \tilde{u}, \bar{p}, \tilde{T}$ )
  - ▷  $\bar{u}, \bar{T}$  not computable (but molecular terms  $\bar{q}$ ,  $\bar{g}$  and  $\bar{q} \cdot \bar{u}$  are non-linear and thus non-computable anyway).



## Compressible LES Formulations (8/19)

- Density-weighted variables (cont'd)
  - ▷ (pointwise) exact mass preservation ensured: continuity equation (46a) becomes

$$\frac{\partial \bar{\rho}}{\partial t} + \operatorname{div}(\bar{\rho} \bar{u}) = 0 \quad (14)$$

- ▷ subgrid-stress tensor

$$\begin{aligned} \underline{\underline{\tau}} &= -\bar{\rho} \underline{\underline{u}} \otimes \underline{\underline{u}} + \bar{\rho} \bar{u} \otimes \bar{u} \\ &= -\bar{\rho} (\bar{u} \otimes \bar{u} - \bar{u} \otimes \bar{u}) \end{aligned} \quad (15)$$



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## Compressible LES Formulations (10/19)

- Density-weighted variables, 3 ways out (cont'd)
  1. Replace (46c) by non-conservative

$$\frac{\partial \bar{\rho}e}{\partial t} + \operatorname{div} [\bar{\rho}e\bar{u} + \bar{q}] = -\bar{p} \operatorname{div} \bar{u} + \underline{\underline{\sigma}} : \underline{\underline{\operatorname{grad}}} \bar{u} \quad (17)$$

(Moin *et al.*, 1991 *Phys. Fluids A*, **3** (11)) or (Erlebacher *et al.*, 1992, *J. Fluid Mech.*, **238**)

$$\frac{\partial \bar{\rho}h}{\partial t} + \operatorname{div} [\bar{\rho}e\bar{u} + \bar{q}] = \frac{\partial \bar{p}}{\partial t} - \bar{p} \operatorname{div} \bar{u} + \underline{\underline{\sigma}} : \underline{\underline{\operatorname{grad}}} \bar{u} \quad (18)$$

## Compressible LES Formulations (9/19)

- Density-weighted variables (cont'd)
  - ▷ filtered total (or stagnation) energy

$$\begin{aligned} \overline{\rho E} &= \bar{\rho} C_v \tilde{T} + \frac{1}{2} \bar{\rho} \bar{u} \cdot \bar{u} - \frac{1}{2} \operatorname{tr}(\underline{\underline{\tau}}) \\ &= \frac{\bar{p}}{\gamma - 1} + \frac{1}{2} \bar{\rho} \bar{u} \cdot \bar{u} - \frac{1}{2} \operatorname{tr}(\underline{\underline{\tau}}) \end{aligned} \quad (16)$$

- ▷ weakly-compressible two-scale DIA expansions (Yoshizawa, 1986, *Phys. Fluids*, **29**, 2152.) suggest model for  $-\frac{1}{2} \operatorname{tr}(\underline{\underline{\tau}})$
- ▷ adequation to more compressible situations questioned by Speziale *et al.* (1988, *Phys Fluids*, **31** (4), 940-942.).
- ▷ Three ways out



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## Compressible LES Formulations (11/19)

- Density-weighted variables, 3 ways out (cont'd)
  1. (cont'd), with internal energy
  $\rho e = C_v \rho T = \frac{p}{\gamma - 1}$  or (static) enthalpy  
 $\rho h = \rho e + p = C_p \rho T = \frac{\gamma p}{\gamma - 1}$ .
  2. add transport equation of resolved kinetic energy (RKE), i.e.  $\frac{1}{2} \bar{\rho} \bar{u} \cdot \bar{u}$  to (17) or (18) (Lee, 1992, Kuerten *et al.*, 1992, Vreman *et al.*, 1995, System I)
    - ▷ non-conservative terms  $-\bar{p} \operatorname{div} \bar{u}$  and  $+\underline{\underline{\sigma}} : \underline{\underline{\operatorname{grad}}} \bar{u}$  remain, along with RKE's contribution  $\bar{u} \cdot \operatorname{div} (\underline{\underline{\tau}})$
    - ▷ successful, e.g. in channel flow  $M = 1.5$ ,  $Re_\tau = 222$  (Lenormand *et al.*, 2000, *AIAA J.*, **38**, 8)



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## Compressible LES Formulations (12/19)

- Density-weighted variables, 3 ways out (cont'd):
  - keep fully conservative (46c) and lump  $\text{tr}(\underline{\underline{\tau}})$  with the filtered internal energy. → modified (and computable) pressure and temperature  $\check{p}$  and  $\check{T}$ : (Vreman *et al.*, 1995, System II)

$$\overline{\rho E} = \bar{\rho} C_v \check{T} + \frac{1}{2} \bar{\rho} \underline{\underline{u}} \cdot \underline{\underline{u}} = \frac{\check{p}}{\gamma - 1} + \frac{1}{2} \bar{\rho} \underline{\underline{u}} \cdot \underline{\underline{u}}, \quad (19)$$

$$\boxed{\check{p} = \bar{p} - \frac{\gamma-1}{2} \text{tr}(\underline{\underline{\tau}}) \quad , \quad \check{T} = \check{p}/(\bar{\rho} R)} \quad . \quad (20)$$

- ▷ counterpart of *macro-pressure*  $\bar{p} - \frac{1}{3} \text{tr}(\underline{\underline{\tau}})$  in incompressible LES with eddy-viscosity assumption  $\underline{\underline{\tau}}_D \simeq 2\bar{\rho}\nu_t \underline{\underline{\underline{s}}}_0$ , with  $\underline{\underline{\tau}}_D = \underline{\underline{\tau}} - \frac{1}{3} \text{tr}(\underline{\underline{\tau}})$ .



## Compressible LES Formulations (14/19)

- 3rd way out: macro-temperature closure (cont'd):
  - ▷ neglecting it in air is 3.75 less stringent than approximation  $\gamma M_{sgs}^2 \ll 1$  required to neglect  $-\frac{1}{2} \text{tr}(\underline{\underline{\tau}})$  with respect to  $\bar{p}$  (see Erlebacher *et al.*, 1992, in a non-conservative context).

## Compressible LES Formulations (13/19)

- 3rd way out: macro-temperature closure (cont'd):

▷ Filtered momentum eq. (46b) becomes

$$\frac{\partial \bar{\rho} \check{u}}{\partial t} + \underline{\underline{\text{div}}} \left[ \bar{\rho} \check{u} \otimes \check{u} + (\check{p} - \frac{5-3\gamma}{6} \text{tr}(\underline{\underline{\tau}})) \underline{\underline{I}} - \underline{\underline{\tau}}_D - \underline{\underline{\sigma}} \right] = 0$$

▷  $\frac{5-3\gamma}{6} \text{tr}(\underline{\underline{\tau}}) = 0$  in monoatomic gases ( $\gamma = 5/3$ ).

▷  $\frac{5-3\gamma}{6} \text{tr}(\underline{\underline{\tau}})/\check{p} = \frac{5-3\gamma}{3} \gamma M_{sgs}^2$ . with  $M_{sgs}^2 = \frac{1}{2} |\text{tr}(\underline{\underline{\tau}})|/\bar{\rho} c^2 = \frac{1}{2} |\text{tr}(\underline{\underline{\tau}})|/(\gamma \check{p})$ .



## Compressible LES Formulations (15/19)

- Density-weighted variables (cont'd): closure of total enthalpy flux  $\overline{(\rho E + p) \underline{\underline{u}}}$ 
  - ▷ resolved pressure:  $\check{p} = \check{p}$  or  $\bar{p}$
  - ▷ at least three levels of decomposition are possible:

$$\overline{(\rho E + p) \underline{\underline{u}}} = (\overline{\rho E} + \check{p}) \check{u} - \underline{\underline{Q}}_H \quad (21)$$

with



## Compressible LES Formulations (16/19)

- Density-weighted variables (cont'd): closure of total enthalpy flux  
 $\overline{(\rho E + p)\underline{u}}$  (cont'd)

$$\underline{\mathcal{Q}}_H = \left[ -\overline{(\rho E + p)\underline{u}} + (\overline{\rho E} + \check{p})\underline{\tilde{u}} \right] \quad (22)$$

$$\begin{aligned} &= \underbrace{\left[ -\overline{(\rho e + p)\underline{u}} + (\overline{\rho e} + \check{p})\underline{\tilde{u}} \right]}_{\underline{\mathcal{Q}}_h} + \\ &\quad \underbrace{\left[ -\frac{1}{2}\overline{\rho(\underline{u}\cdot\underline{u})\underline{u}} + \frac{1}{2}(\overline{\rho}\underline{u}\cdot\underline{u})\underline{\tilde{u}} \right]}_{\mathcal{W}} \end{aligned} \quad (23)$$



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## Compressible LES Formulations (17/19)

- Normand and Lesieur (1992) heuristic form

$$\begin{aligned} \frac{\partial \overline{\rho}}{\partial t} + \underline{\text{div}}(\overline{\rho}\underline{u}) &= 0 \\ \frac{\partial \overline{\rho}\underline{u}}{\partial t} + \underline{\text{div}}\left(\overline{\rho}\underline{u} \otimes \underline{u} + \check{p}\underline{I} - 2[\mu(\check{T}) + \overline{\rho}\nu_t(\underline{u})]\underline{\underline{S}_0}(\underline{u})\right) &= 0 \\ \frac{\partial}{\partial t}\left(\frac{\check{p}}{\gamma-1} + \frac{1}{2}\overline{\rho}\underline{u}\cdot\underline{u}\right) + \underline{\text{div}}\left[\left(\frac{\gamma}{\gamma-1}\check{p} + \frac{1}{2}\overline{\rho}\underline{u}\cdot\underline{u}\right)\underline{u} - C_p\left(\frac{\mu(\check{T})}{Pr} + \frac{\overline{\rho}\nu_t(\underline{u})}{Pr_t}\right)\underline{\text{grad}}\check{T} - 2\mu(\check{T})\underline{\underline{S}_0}(\underline{u})\cdot\underline{u}\right] &= 0 \end{aligned} \quad (25)$$

still with  $\check{T} = \check{p}/(\overline{\rho}R)$ .

## Compressible LES Formulations (17/19)

- Density-weighted variables (cont'd): closure of total enthalpy flux  
 $\overline{(\rho E + p)\underline{u}}$  (cont'd)

$$\underline{\mathcal{Q}}_h = \underbrace{\left[ -\overline{(\rho e)\underline{u}} + (\overline{\rho e})\underline{\tilde{u}} \right]}_{\underline{\mathcal{Q}}_e} + [-\overline{p}\underline{u} + \check{p}\underline{\tilde{u}}] \quad (24)$$

$\rho e = \rho C_v T = p/(\gamma - 1)$ : internal energy.

- $\underline{\mathcal{Q}}_h$  and  $\underline{\mathcal{Q}}_e \propto \underline{\text{grad}}\check{T}$  (in Erlebacher *et al.*, 1992, and Moin *et al.*, 1991, resp.)
- $\underline{\mathcal{Q}}_H \simeq \overline{\rho}C_p(\nu_t/Pr_t)\underline{\text{grad}}\check{T}$  with  $\check{p} = \check{p}$  yields Normand and Lesieur (1992):



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## Compressible LES Formulations (19/19)

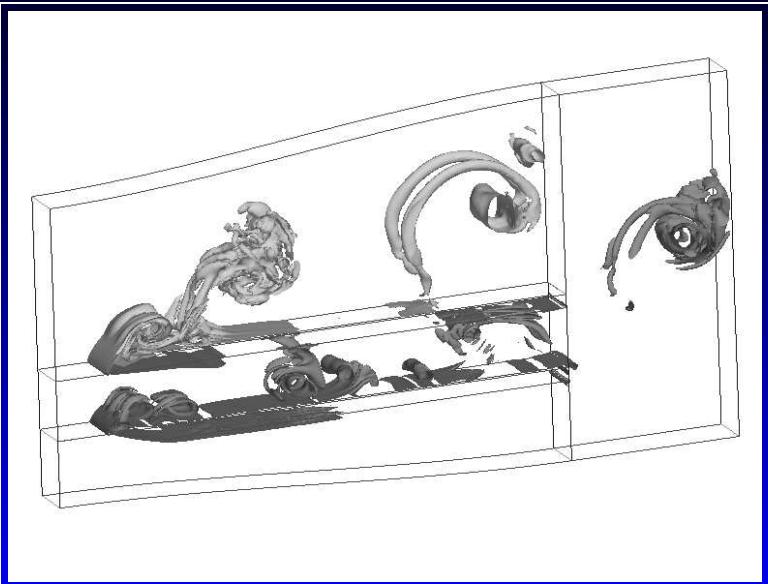
- Normand and Lesieur (1992) heuristic form (cont'd)
  - amounts to adding  $\overline{\rho}\nu_t$  and  $\overline{\rho}C_p(\nu_t/Pr_t)$  to their molecular counterpart in (25) except in the last term of the energy equation.
  - This exception disappears when option (62b) is taken, with  $\underline{\mathcal{Q}}_h \simeq \overline{\rho}C_p(\nu_t/Pr_t)\underline{\text{grad}}\check{T}$  and the RANS type model  $\mathcal{W} \simeq \underline{\tau}\cdot\underline{\tilde{u}}$ .
  - used successfully by Knight *et al.* (1998, see also Okong'o & Knight, 1998) on unstructured grids.
  - $|\mathcal{W} - \underline{\tau}\cdot\underline{\tilde{u}}|$  small in constant-density RANS filtering.



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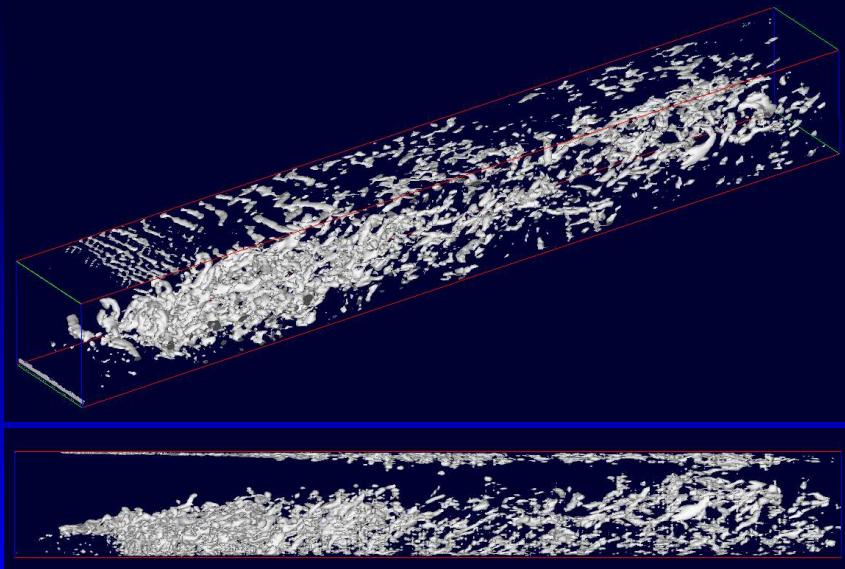
## Air intake, Arnaudon & Tsen, 1974 (1 of 5)



Low  $Re$  number. Isosurface of vorticity magnitude for  $\theta = 30^\circ$ .

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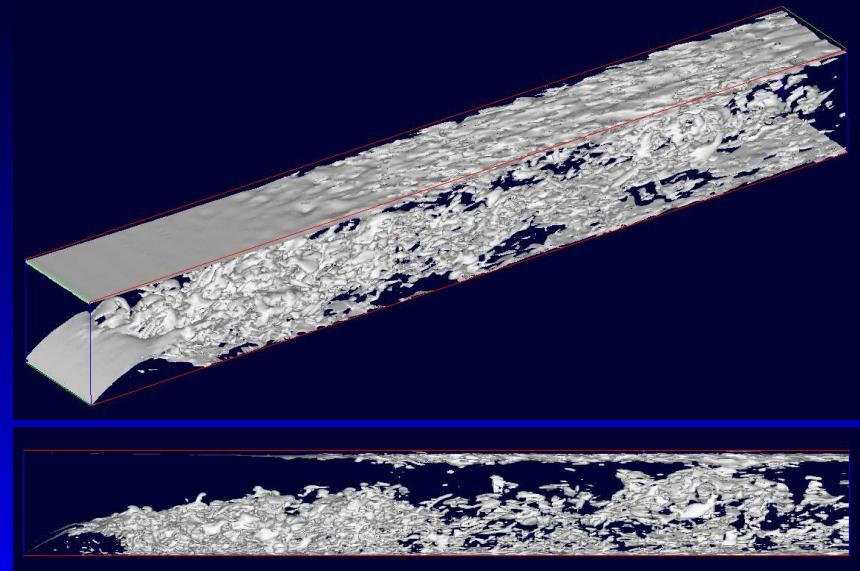
## Air intake (3 of 5)



$Re = 50000$ . Iso-surface  $Q = \frac{1}{2}(\Omega_{ij}\Omega_{ij} - S_{ij}S_{ij}) = 0.4 (U_\infty/H)^2$

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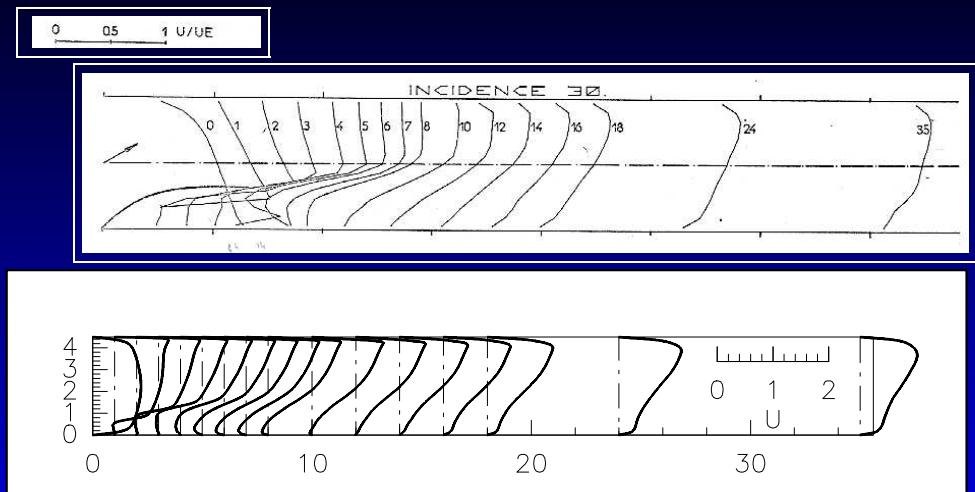
## Air intake (2 of 5)



$Re = 50000$ . Isosurface of vorticity magnitude:  $\|\vec{\omega}\| = 1.1 U_\infty/H$

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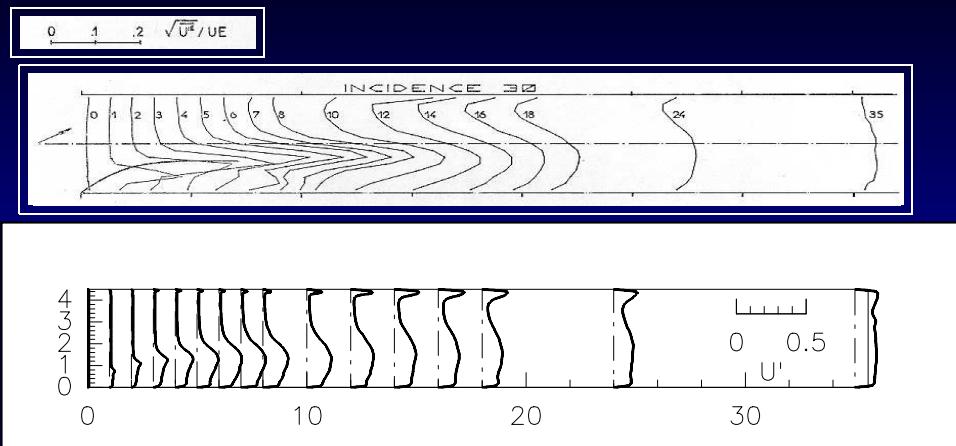
## Air intake (4 of 5)



$\theta = 30^\circ$ :  $\bar{u}$  Arnaudon & Tsen (1974) top

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## Air intake (5 of 5)



$\theta = 30^\circ$ :  $u'$  Arnaudon & Tsen (1974) top